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Measuring the Corrosion Rate of Reinforcing Steel in Concrete

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National Bureau of Standards
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U.S. DEPARTMENT OF COMMERCE, Malcolm Baldrige, *Secretary*
NATIONAL BUREAU OF STANDARDS, Ernest Ambler, *Director*

MEASURING THE CORROSION RATE OF REINFORCING STEEL IN CONCRETE

The deterioration of concrete bridge decks as a result of corrosion action on the reinforcing steel is a serious and costly problem to the nation (1). It is recognized that this corrosion is caused by the diffusion of chloride ions into the concrete resulting in the breakdown of the passive iron oxide film that normally protects the steel. The corrosion product that forms generates sufficient pressure to crack the concrete allowing moisture, oxygen, and more chloride to enter, further accelerating the deterioration process (2).

Methods have been developed that: a) block the chloride from coming in contact with the steel, (b) stop the chloride from entering the concrete, (c) remove the chloride from the vicinity and (e) others, such as cathodic protection, which modify the reactions at the surface of the steel (3-7). All of these approaches require some method to evaluate their effectiveness, and the most direct method is to measure the corrosion rate of the steel before and after a modification to the concrete.

Procedure

The plan for this study is divided into the following five phases which are: A literature review, preliminary studies, measurements in concrete, field measurements, and the development of a microprocessor system. More than half of these phases have been accomplished and reported as will be described.

Phase I. Literature Review - At the outset, a literature search was undertaken to identify the information available on the corrosion of steel in concrete and methods for measurement. A total of 394 papers, reports, and talks from 1964 through 1978 were identified on the subject, and are indexed under subject and author (8). The Subject Index was further subdivided into six subgroups such as general survey, factors affecting corrosion, measurement

techniques, protection techniques, concrete design, and related fields. In the Author Index, the references are listed alphabetically by author.

A study of this literature revealed several interesting facts. For example, it was found that over thirty references discussed the effect of chloride on corrosion, but only one reference discussed the effect of oxygen content. Furthermore, the effect of moisture was considered in just four of these references. Not one study on the corrosion of steel in an alkaline environment was found. Clearly, most of the attention had been directed towards the effects of chloride.

Phase II. Preliminary Studies - From the information gathered through the literature search, it was evident that more information was needed on the effects of oxygen, pH, and moisture, and therefore an experimental program was designed to evaluate these factors. Three environments were used on this phase of the study, and these were alkaline solutions of Ca(OH)_2 with controlled oxygen, Cl^- , and pH; wet sand/salt mixtures; and mortar (9).

Flat steel specimens 100 x 20 x 1 mm were immersed in controlled solutions and the initiation time for visible corrosion was noted. At a pH of 10.5 or less, corrosion started immediately on immersion. However, as the pH was raised to 12, initiation times increased to 200h, and at higher pH corrosion did not occur during the period of the experiment. The experiment was repeated in the presence of chloride, and it was found that chloride did reduce the initiation time to corrosion but otherwise had little effect. Once initiated, the corrosion rates were constant in all cases. Not surprisingly, the oxygen content of the solution had a large effect on the corrosion rate of the steel with lower concentrations leading to lower corrosion rates.

Further experiments were carried out as described which indicated that the interaction of oxygen, pH, and chloride is more complex and in combination can develop conditions that lead to corrosion even at high values of pH. Figure 1 is a summary of these data showing these three parameters. Illustrated is a three dimensional figure with boundaries within which corrosion does not occur. However, outside of this boundary corrosion of steel is observed. For example, where it was shown earlier that chloride or oxygen acting alone could not cause corrosion of steel at a pH of 12.5, this figure reveals that at an oxygen concentration as low as 2 ppm and at a Cl^- concentration of 6 mol/l, corrosion does occur, and can also develop at lower concentrations of Cl^- at higher oxygen contents.

To observe the effect of moisture on the corrosion of steel, specimens were imbedded in a mixture of sand, $\text{Ca}(\text{OH})_2$, and NaCl. The mixture was held in small perforated crucibles in an atmosphere of flowing air with controlled moisture content. This configuration allowed the specimens to be removed for weight loss determination during the course of the experiment. Specimens in a moisture saturated sand mixture did not corrode, but during the same period, specimens in a dry mixture began to corrode almost immediately as moisture was introduced. However, the corrosion rate of these specimens decreased steadily as moisture content of the sand mixture increased; and at saturation, the corrosion ceased. Clearly, the degree of moisture, which affects oxygen concentration, plays a very important role as expected, but the cessation of corrosion at saturation was not anticipated.

After the study of steel in solutions and in sand mixtures was completed, the work was extended to include steel in mortar. Specimens as described above were cast with a 5 mm cover of chloride-containing mortar. After 24h, half of the specimens were immersed in a $\text{Ca}(\text{OH})_2/\text{NaCl}$ solution and half

were allowed to dry for one week before immersion. The corrosion current of each specimen was determined by polarizing the specimen from -10 to +10 mV with a potentiostat and plotting the overvoltage as a function of the polarizing current. As in the case of the sand mixture, the corrosion of the steel in mortar that was kept continuously wet was near zero, but the specimens that were allowed to dry for one week, and then immersed, initially developed a high corrosion rate that decreased with time to a very low value.

In summary, these studies have shown that at low concentrations of O_2 and Cl^- , pH controls the initiation of corrosion. But as O_2 and Cl^- increase, corrosion can initiate even at a pH of 12.5. It is hypothesized that in the moisture saturated concrete, the concentrations of Cl^- and oxygen are sufficiently low for conditions to exist within the "no corrosion" boundary of Figure 1. However, as the concrete dries, the Cl^- concentration in the pore water eventually increases to saturation. This drying process also allows oxygen to diffuse more rapidly through the concrete setting up conditions outside of the "no corrosion" boundary where corrosion of steel does take place. Once corrosion is initiated, the pH is reduced at the anodic areas by the corrosion reaction, making it easier to reinitiate corrosion in future times when moisture and oxygen are available.

Phase III. Measurements in Concrete - The purpose of this portion of the work was to compare several polarization techniques for measuring the rate of corrosion of steel in concrete(9). All polarization techniques are essentially the same in that the measurement is based on the observation that the polarizing current necessary to change the potential of a metal in an electrolyte, in this case concrete, is directly related to the rate of corrosion of the metal. The techniques differ only by how this change

in potential is achieved. Initially, four techniques were used in this study and are described as follows: Stern and Geary consider the derivative of the potential of the specimen versus the applied current for deviations from the corrosion potential not greater than 10 mV (10). This slope is related to the corrosion current, I_{CORR} , by the relationship:

$$\lim_{dE \rightarrow 0} \frac{dE}{dI} = \frac{b_a \cdot b_c}{2.3(b_a + b_c)I_{CORR}}$$

where b_a and b_c are the anodic and cathodic Tafel Slopes respectively. For calculation of the corrosion current, I_{CORR} , values for the Tafel slopes must be obtained from other sources, or by trial and error for the best fit to the data. In this case ΔE was 6 mV and the assumption made that $b_a = b_c = 100$ mV. Thus:

$$I_{CORR} = \frac{21.7\Delta I}{\Delta E}$$

The second technique used is an empirical approach described by Schwedtfefer in which I_{CORR} is determined from the change in slope of the polarization curve (11). The cathodic corrosion current, I_p , and the anodic corrosion current, I_q , are found at this "break" in the curve, and the corrosion current is then calculated from:

$$I_{CORR} = \frac{I_p I_q}{I_p + I_q}$$

The technique requires that polarization, ΔE , extend over a range of ± 100 mV so that the "breaks" in the polarization curve may be observed.

The three point method of Barnartt is the third technique that has been used (12). Three voltage/current data points are measured along the polarization curve, and from this b_a , b_c , and I_{CORR} are calculated as follows. If the first potential point is at ΔE , then the second and third are at $2\Delta E$ and $-2\Delta E$ respectively. The resulting currents at each potential are measured and substituted into the ratios

$$r_1 = I_{2\Delta E} / I_{-\Delta E}$$

and $r_2 = I_{2\Delta E} / I_{\Delta E}$

which in turn are related to each other through the quadratic equation

$$U^2 - r_2U + r_1 = 0$$

The roots of this equation are

$$\exp \frac{2.3 \Delta E}{b_a} \quad \text{and} \quad \exp \frac{2.3 \Delta E}{b_c}$$

from which b_a and b_c are calculated. Using the relationship of I/I_{corr} versus ΔE , the corrosion current for the process is found.

The fourth technique is a computer analysis of polarization data developed by Mansfield (13). The computer makes a best fit analysis to theoretical curves generated from the Stern-Geary equation for different values of Tafel slopes and in this way b_a , b_c , and I_{corr} are found.

Each of the polarization techniques described employs a three electrode system having the steel specimen as one electrode, a voltage reference as a second electrode, and a counter electrode as a third electrode from which polarizing current is applied to the specimen. The circuit used for these measurements is Holler's (14) which incorporates a Wheatstone bridge for IR compensation as illustrated in Figure 2. The IR compensating design takes advantage of the fact that when a polarizing current is applied to the specimen, its rate of change in potential due to polarization is very small compared to the rate of change in potential due to IR. By repeated applications of current of short duration (e.g. 0.5s), and by adjusting the Wheatstone balancing resistance, the IR component is compensated. Once this balance is achieved, then the polarizing potential, free of IR, can be measured for all values of applied current.

Small concrete slabs 55 x 30 x 5 cm were cast each with three imbedded 1.27 cm diameter steel rods. Two small stainless steel rods were also encased in the concrete and were used to determine the resistivity of the slab. The concrete was treated in two ways. Four of the slabs were cast with 0.06 parts NaCl to one part cement (38.4 lbs NaCl/cu.yd), and the remaining eight slabs were cast without Cl⁻. After curing for approximately thirty days, two of the Cl⁻ free slabs were immersed in a saturated solution of NaCl for six days, withdrawn, and left in a dry laboratory atmosphere. Two other slabs were immersed in a 3.5% NaCl solution for 24h, withdrawn, and also left in a laboratory atmosphere. Corrosion measurements showed that steel specimens in Cl⁻ free slabs developed very low corrosion rates (<0.007 mg/dm²/day). However, those slabs with Cl⁻ in the concrete immediately developed a corrosion rate of 4.4 mg/dm²/day or more than two orders of magnitude greater than those in Cl⁻ free concrete. Figure 3 illustrates the decreasing rate of corrosion as the concrete dried. In the case where the chloride free concrete slabs were immersed for six days in a sodium chloride saturated solution, the corrosion rate increased by over an order of magnitude within a few hours as shown in Figure 4. The second group of chloride free concrete slabs that were immersed for only 24h in a solution of 3.5% NaCl behaved similarly to those immersed longer in a more concentrated solution. The average weight loss of steel on these specimens, based on electrochemical measurements, was 0.33 mg/dm²/day. The resistivity of the concrete was also measured with time, and the data reveal that the resistivity decreases as moisture increases. However, the effect of immersion on the corrosion rate is much greater than its effect on the resistivity of the concrete. As the concrete dries and the resistivity increases above 7,000 ohm-cm, the resistance appears to have a direct influence on the degree of corrosion observed.

Weight losses were calculated from the electrochemically determined corrosion currents measured as a function of time, and were compared to gravimetric weight loss measurements on the same cleaned steel rods. A comparison of the data from the four electrochemical techniques described is shown in Table 1 and indicates that all methods overestimated the weight loss of steel. The Stern-Geary method overestimated weight loss by 17% while Schwerdtfeger's, Mansfeld's, and Barnartt's techniques overestimated weight loss by 40%, 56%, and 83% respectively. Since the differences in the corrosion rates between a corroding and a non-corroding system are over an order of magnitude, then even the data with an overestimation of 83% will reveal the existence of high corrosion.

In summary, the data indicate that the corrosion of steel in chloride free concrete is negligible and less than $0.007 \text{ mg/dm}^2/\text{day}$ while the corrosion rate in chloride contaminated concrete is more than an order of magnitude greater with an average of $0.33 \text{ mg/dm}^2/\text{day}$, but can be as high as $4.4 \text{ mg/dm}^2/\text{day}$. Comparison of the gravimetrically determined weight loss to the weight losses calculate from the polarization data indicates that the electrochemical measurements overestimate weight loss by 17% to 83%. However, even with an overestimation of 83%, the polarization techniques will differentiate between a corroding and a noncorroding condition of steel in concrete.

An important part of this study is the characterization of the current distribution during polarization measurements. This distribution must be known in order to determine the area of the steel being polarized which, in turn, makes it possible to calculate a corrosion current density or weight loss of steel per unit length of steel bar.

Under controlled laboratory conditions, determining this area is not a serious problem since the specimens are small and the geometry of the

electrodes can be arranged so that the entire specimen electrode is polarized with a uniform current. But in extending these polarization measurements to a bridge deck we are faced with limitations brought on by the relatively large size of the structure. The major constraint being that, unlike our small slabs in the laboratory, we cannot polarize the entire bridge at once, but can only polarize a small area at a time, and it is this area that must be characterized.

The experimental procedure used is simple in principle. In an attempt to simulate the large scale geometry in a small slab, it was decided to use a long line specimen in concrete and polarize it from a point or small line current source. The potential of the steel in the concrete would be monitored by reference electrodes positioned along its length.

Three variables were considered as having an effect on the distribution of the current, and these are the distance between the counter electrode and the specimen, the amount of current applied, and the resistivity of the concrete.

Using small concrete slabs similar to those described earlier, a new geometric arrangement of electrodes was designed as shown in Figure 5. As before, the steel rod is imbedded horizontally along the length of the concrete slab. The counter electrode is a small diameter (3 mm) rod positioned vertically adjacent to the steel specimen. Three counter electrodes at different distances (1,2,4cm) from the specimen are illustrated. Ten reference electrodes, imbedded in the concrete, are located 8.5 cm apart along the length of the steel rod and 2 cm from its surface. This arrangement of electrodes allowed a polarizing current to be applied to the steel specimen from a small vertical line source. Any changes along the length of the specimen are detected by the reference electrodes. Measurements were

made using one of the three counter electrodes. The resistivity of the concrete was controlled by controlling its moisture content. During an experimental run, the potential along the length of the specimen was measured before any current was applied. Subsequent potential measurements were made with reference to this initial base potential. The polarizing current was increased in increments and the potential measurements repeated until a maximum of approximately 10 mV was achieved. Initial measurements were made manually using the Holler bridge circuit for compensation of IR. More recent measurements were made using a computer controlled system which applies a cycling direct current of 5 seconds on and 0.25 seconds off. The potential of the specimen was then read during the current off cycle so that the IR component was zero. Figure 6 illustrates the distribution of current as indicated by the change in potential along the length of a steel rod in concrete. This curve is a measure of the extent of current distribution along the length of a horizontal steel rod when the current source is a small vertical rod in the concrete. The shape of the curve is an indication of how uniformly the current is distributed within the polarized area. This type of data have been obtained as a function of counter electrode distance, applied current, and resistivity of concrete. Preliminary analysis of the data indicates that, as expected, the extent of the current distribution decreases as the resistivity of the concrete increases, and the general shape of the current distribution curve does not appear to be affected. In addition, as the electrode distance is decreased, the area of steel rod polarized also decreases. The largest effect observed is that of the applied current. As the current is increased, the area of distribution

increases. But perhaps the most important observation is that current distribution is very limited and 90% of the current encompasses a distance of less than 10x the distance between the specimen and the current source electrode.

A mathematical model has been developed that takes these variables into consideration and generates a current distribution curve along a cylinder from a point source in free space as follows. The electric current distribution in a conductive medium containing electrodes held at arbitrarily fixed potentials may be obtained by a standard application of potential theory. For the case of an infinitely long cylindrical conductor embedded in an electrolyte with a point source of current at a fixed distance from the cylinder, an extension of the formulas given by Jackson gives a complete solution for the current distribution in the electrolyte (15).

The following geometric arrangement is treated as illustrated in Figure 7. Consider an infinitely long metallic cylinder of radius a , held at ground potential, and at a distance, d , from the axis of the cylinder, a point electrode emits a total current I_0 . By application of the methods stated above, the current density at any point, P , on the surface of the cylinder is described.

$$J(Z, \theta) = \frac{I_0}{\pi^2 a} \sum_{m=0}^{\infty} \frac{\cos m\theta}{\epsilon_m} \int_0^{\infty} dk \cos kz \frac{K_m(kd)}{K_m(ka)}$$

where

- $J(Z, \theta)$ = Current density at point P on the cylinder
- I_0 = Total current emitted by source at d
- m = Integer index for summation
- k = Variable of integration
- ϵ_m = 2 for $m = 0$; 1 for $m > 0$
- $K_m(x)$ = A modified Bessel function of the second kind, order m , argument x , see ref. (16)

Although this formula is a closed mathematical expression with a precisely defined meaning, its evaluation to a specified accuracy requires numerical integration of a function which is rapidly oscillating and the summation of a convergent series. Use of digital computing methods to produce graphical or tabular representation of the results is essential. A preliminary evaluation of the function, illustrated in Figure 8, demonstrates that it does follow the general shape of the measured data. Further analysis of this function and its correlation to the data is required for a more accurate assessment of their relationship.

Phase IV. Field Measurements - After gaining some experience in performing the corrosion measurements on concrete slabs in the laboratory, the measurements were extended to the field on an operating bridge deck. With the cooperation of the Virginia Highway Department arrangements were made to perform corrosion rate measurements on a bridge deck (Number 2063) on Interstate 66 near the Washington, DC Beltway. The primary objective of this portion of the study was to evaluate the background electrical noise and determine whether the measurements could be made.

Measurements were made on two separate decks that were a few hundred meters apart. Two sets of measurements were made on a seven year old deck (area A) repaired and widened (area B) eighteen months earlier and now in use, and one set was made on a deck (area C) over a year old but not yet opened to traffic. The major difference between the two decks is that the older deck with its new widened section had been exposed to de-icing salts while the new deck, barricaded to traffic, was not salt contaminated.

During the measurements, electrical contact was made to the steel rebar with modified locking pliers. The counter electrode was a 500 cm² rectangle of aluminum foil wrapped in a towel wetted with a saturated solution of

Ca(OH)_2 . A 6. cm diameter hole was cut out of the center of the counter electrode to accommodate the Cu/CuSO_4 reference electrode positioned at this point on a small wetted sponge. Using the Stern-Geary technique and the Holler bridge circuit, measurements were made at areas A, B, and C, and a portable Tetronix Model 214 oscilloscope was employed to monitor the background electrical noise.

The background electrical noise was found to be a very high frequency signal beyond the kilohertz range of our instrument, but more importantly, it was of very low amplitude and less than 1 mV. Apparently the steel structure of the deck acts as a very good antenna for radio frequency radiation. The corrosion measurements revealed that area A on the 7 year structure developed a corrosion current of 9.8 μA , while area B on the recently widened section of the same structure had a corrosion current of 6.9 μA . The new deck not open to traffic displayed the lowest corrosion current of 1.2 μA . Thus, though the data could not be verified by examination of the steel, it did seem reasonable. That is the oldest contaminated structure did display the highest corrosion and the new uncontaminated deck the lowest corrosion. Furthermore, it was found that the measurements could be made and that background interference was negligible.

Phase V. Microprocessor System - It is recognized that the corrosion measurements are tedious, time consuming, and require some knowledge of the concepts involved, and because these measurements lend themselves to automation, the ultimate goal of this project is to develop an instrument that will make these measurements automatically. Field measurements would then be performed with a microprocessor controlled device which would relieve the operator of most of the detailed adjustment, data acquisition, and calculations required. This device is to be as simple

allowing minimally trained personnel to perform the measurements. A description of the design of such a device follows.

The instrument is designed around a set of commercially available microcomputer printed circuit cards. These are based on a MC 6809 micro-processor circuit giving the system a very capable and powerful controller. The modules used in the system are:

- 1.) The processor card
- 2.) Battery backed-up memory
- 3.) Serial, parallel, and timing card
- 4.) Analog to digital converter
- 5.) Digital to analog converter (modified)
- 6.) Vacuum fluorescent display

In addition to these commercial cards, several other cards have been constructed at NBS, and serve two functions. First, to provide an interface between the user and the system are the following:

- 1.) Keyboard and display panel
- 2.) Test and keyboard control

Second, to interface the instrument to the experimental cell, these cards were constructed:

- 3.) Voltage to current converter
- 4.) Input amplifier and distribution card

Schematics of these cards and the modification to the digital to analog converter are illustrated in Figures 9 through 13.

The instrument operates in the following manner. At turn on, if the test switch is on, the unit is in a display test mode. The system will not function except for the display which will demonstrate the full character

set on a character by character basis. When the test switch is deactivated, followed by a reset, the system goes into operational mode and instruction messages appear on the display.

In the operational mode, the processor requests information from the user, and when all necessary parameters are stored, sets up the system for zero levels and enters a wait state until the operator lets it know that final hook up to the cell is complete. This information is transmitted to the instrument by pressing the "RUN" key thereby activating the microprocessor to begin data acquisition. Output current is generated by a precision voltage to current converter. Voltage driving this converter is derived from a 10 bit digital to analog converter under control of the processor. The full scale output current range is also selectable by the processor software. Input potentials are measured by a 12 bit analog to digital converter. Three channels are used in this measurement. One channel measures the current applied, another the counter electrode to working electrode potential, and the third the reference electrode to working electrode potential where the working electrode is steel in the concrete. The data are then saved in a battery backed up memory remaining there until deliberately erased. When data acquisition is complete, calculations are performed and the results displayed. A permanent record can then be printed out and the data erased, or another experiment can be performed while the data is saved for later printing. The software has been developed as a system of modular routines, the majority of which are single function stand alone subroutines (Appendix A). Links between modules have been made absolute, and therefore the overall program is not relocatable. However, relocation can be put into the system with little difficulty, if it should prove desirable. The software design is such that changes to the

measurement technique can be made by changing 3 or 4 of the modules. Such a change is necessary to the present modules since interfacing problems have resulted in an error in the measurements. These changes are in the process of being implemented.

Summary

This National Bureau of Standards study has revealed the following information.

1.) A total of 394 papers, reports, and talks from 1964 to 1978 were found pertinent to the subject of the corrosion of steel in concrete. A study of this literature indicated that information was lacking on the effect of oxygen, pH, and moisture.

2.) Oxygen concentration, chloride concentration, and pH have been found to control the initiation of the corrosion of steel in concrete. Moisture content of the concrete also plays an important role through its effect on the concentration of oxygen and chloride.

3.) The comparison of four polarization techniques for measuring the corrosion of steel in concrete reveals that all the techniques overestimated the weight loss from 17 to 83%. Current distribution measurements indicate that the extent of current distribution along a steel bar in concrete is very limited and of the order of 10 times the distance between the specimen and the current source. A mathematical model describing this current distribution is being developed.

4.) Corrosion rate measurements on operating bridge decks verify that polarization techniques can be used in this situation, and furthermore, background electrical noise is negligible.

5.) A microprocessor controlled instrument for making corrosion rate measurements has been designed and constructed. However, complications in interfacing the cards have developed requiring a change in its design. These improvements are in the process of implementation.

REFERENCES

1. An Economic Analysis of the Environmental Impact of Highway Deicing, U. S. Environmental Protection Agency, EPA-600/276105, May 1976.
2. Cornet, I., Bresler, B., Galvanized Steel in Concrete: Literature Review and Assessment of Performance, Galvanized Reinforcement for Concrete-II, International Lead Zinc Research Organization, Inc., Vol. 2, May 1981.
3. Clifton, J. R., Protection of Reinforcing Bars with Organic Coatings, Materials Performance, 15, No. 5, 14-17, May 1976.
4. Internally Sealed Concrete Guide to Construction and Heat Treatment, Federal Highway Administration, Implementation Package 77-9, April 1977.
5. Slater, J. E., Lankard, D. R., Moreland, P. J., Electrochemical Removal of Chlorides from Concrete Bridge Decks, Materials Performance, 15, 11, 21-26, 1976.
6. Lundquist, J. T., Rosenberg, A. M., Gaidis, J. M., Calcium Nitrite as an Inhibitor of Rebar Corrosion in Chloride Containing Concrete Materials Performance, 18, 36-40, March 1979.
7. Fromm, H. J., Wilson, G. P., Cathodic Protection of Bridge Decks: A Study of Three Ontario Bridges, Transportation Research Board, Transportation Research Record No. 604, 38-47, 1976.
8. Escalante, E., ITO, S., A Bibliography on the Corrosion and Protection of Steel in Concrete, National Bureau of Standards Special Publication 550, August 1979.
9. Escalante, E., Ito, S., Cohen, M., Measuring the Rate of Corrosion of Reinforcing Steel in Concrete, National Bureau of Standards NBSIR 80-2012, March 1980.
10. Stern, M., Geary, A. L., A Theoretical Analysis of the Shape of Polarization Curves, J. Electrochemical Society, 104, 56, January 1957.
11. Schwerdtfeger, W. J., McDorman, O. N., Measurement of the Corrosion Rate of a Metal From Its Polarization Characteristics, J. Electrochemical Society, 99, 407, October 1952.
12. Barnartt, S., Two-Point and Three-Point Methods for the Investigation of Electrode Reaction Mechanisms, Electrochimica ACTA, 15, 1313, 1970.
13. Mansfeld, F., Tafel Slopes and Corrosion Rates from Polarization Resistance Measurements, Corrosion, 29, No. 10, October 1973.
14. Holler, H. D., Studies of Galvanic Couples, J. Electrochemical Society, 97, 271, September 1950.
15. Jackson, J.D., Classical Electrodynamics, John Wiley and Sons, N.Y., 84, 1962.
16. Handbook of Mathematical Functions with Formulas, Graphs, and Mathematical Tables, National Bureau of Standards, Applied Mathematics Series No. 55, 1964.

TABLE 1
 Comparison of Weight Loss Determined Gravimetrically
 to
 Weight Loss Calculated From Polarization Data

Technique	Weight Loss, mg	Overestimate %
Gravimetric	147	--
Stern-Geary	172	17
Schwerdtfeger	206	40
Mansfeld	230	57
Barnartt	269	83

FIGURES

- 1.) A three dimensional plot of Cl^- concentration, oxygen concentration, and pH showing the regions of corrosion and no corrosion.
- 2.) A simplified schematic of the Holler bridge circuit as used in a manual measurement of corrosion rate of steel in a concrete slab.
- 3.) A plot of corrosion current and resistivity versus time for steel in salt contaminated concrete.
- 4.) A plot of corrosion current and resistivity versus time for steel in concrete contaminated with salt after curing.
- 5.) Geometry of electrodes for current distribution measurements.
- 6.) A plot of current distribution along a steel bar in concrete as indicated by its change in potential.
- 7.) Geometry of electrodes used in model of the current distribution calculation.
- 8.) A plot of one half of the current distribution along an infinitely long cylinder as calculated from the model.
- 9.) Schematic diagram of the keyboard and display panel circuit.
- 10.) Schematic diagram of the keyboard and display panel circuit.
- 11.) Schematic diagram of the keyboard scanner circuit.
- 12.) Schematic diagram of the voltage to current converter circuit.
- 13.) Schematic diagram of the input amplifier and distribution circuit.

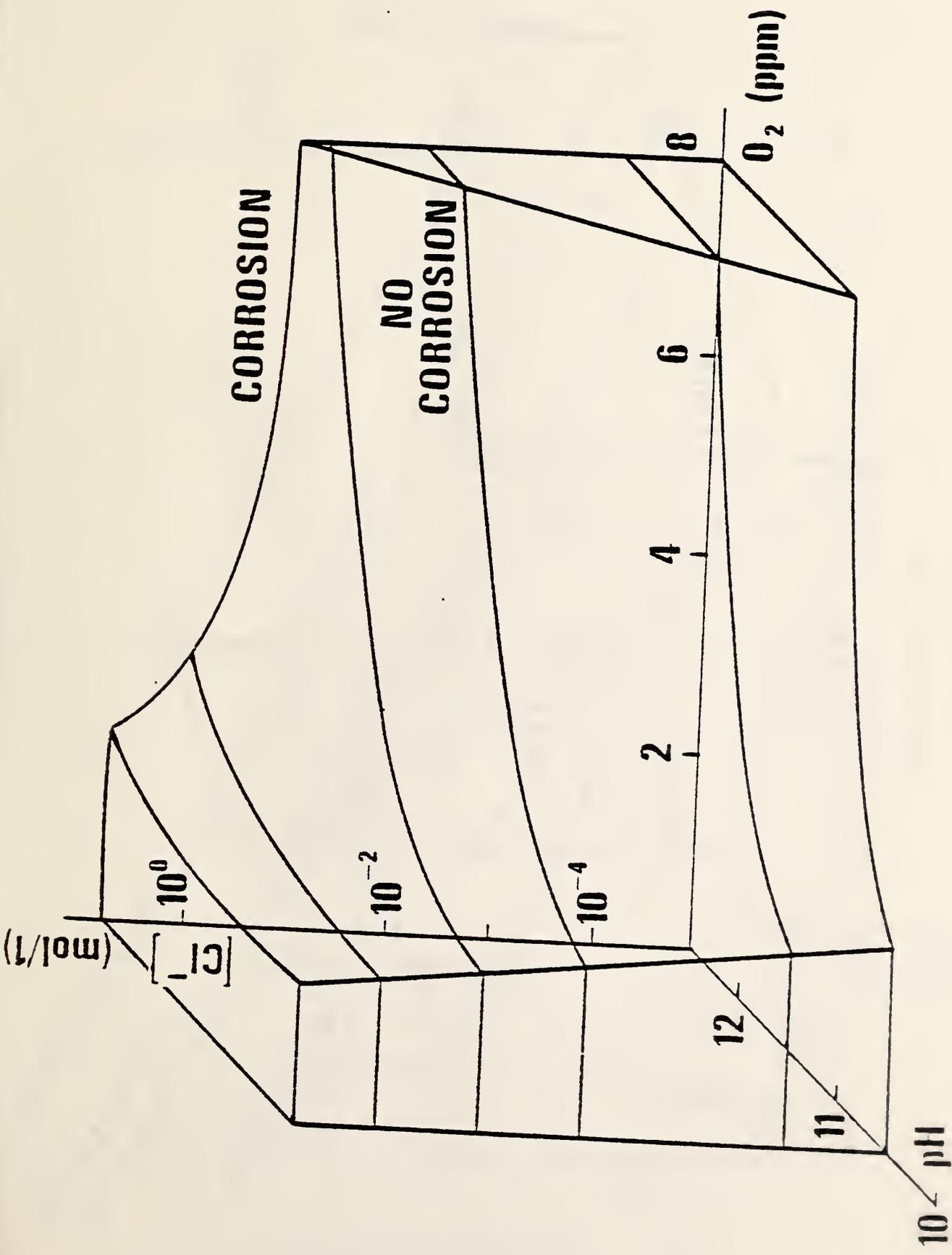


Figure 1

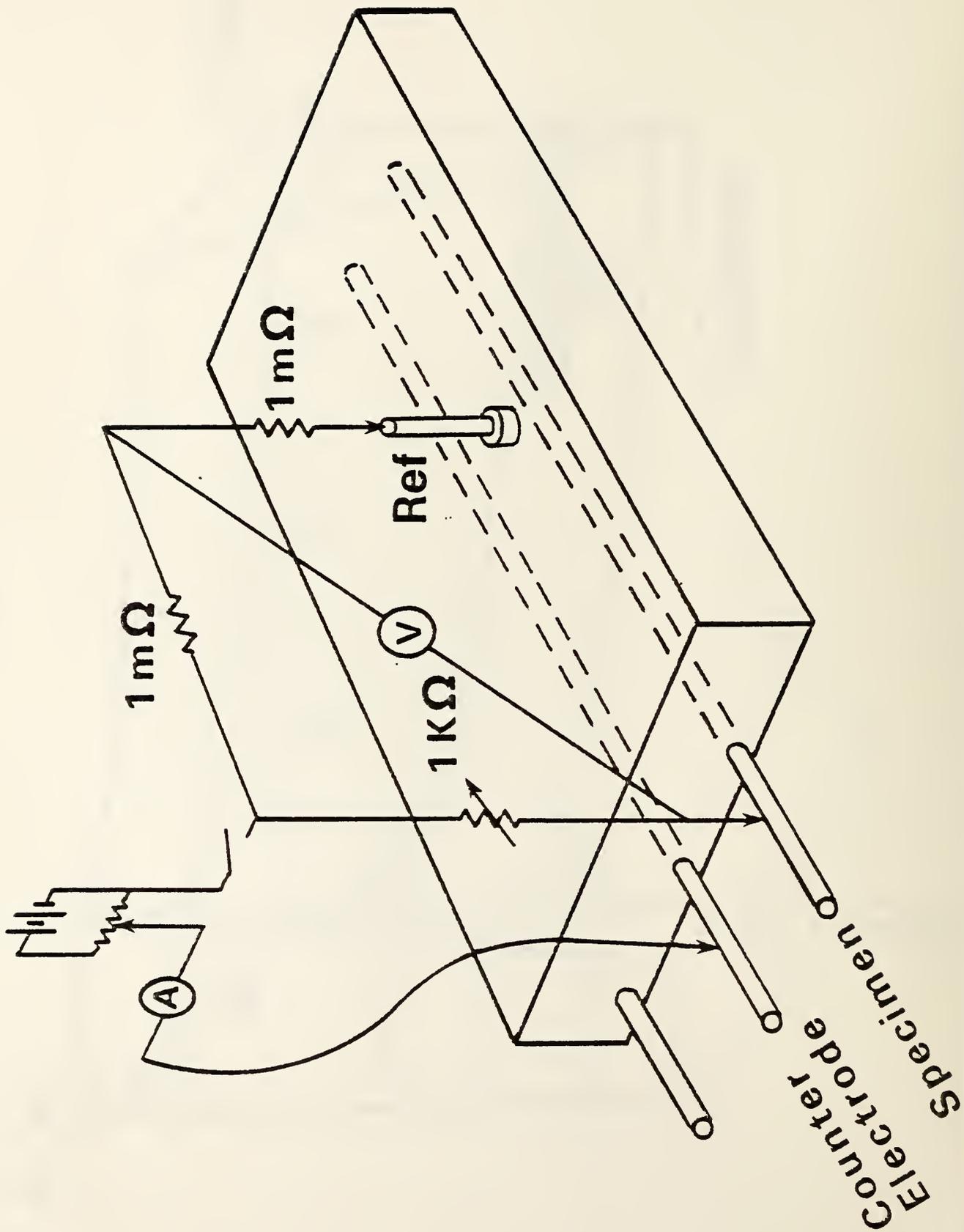


Figure 2

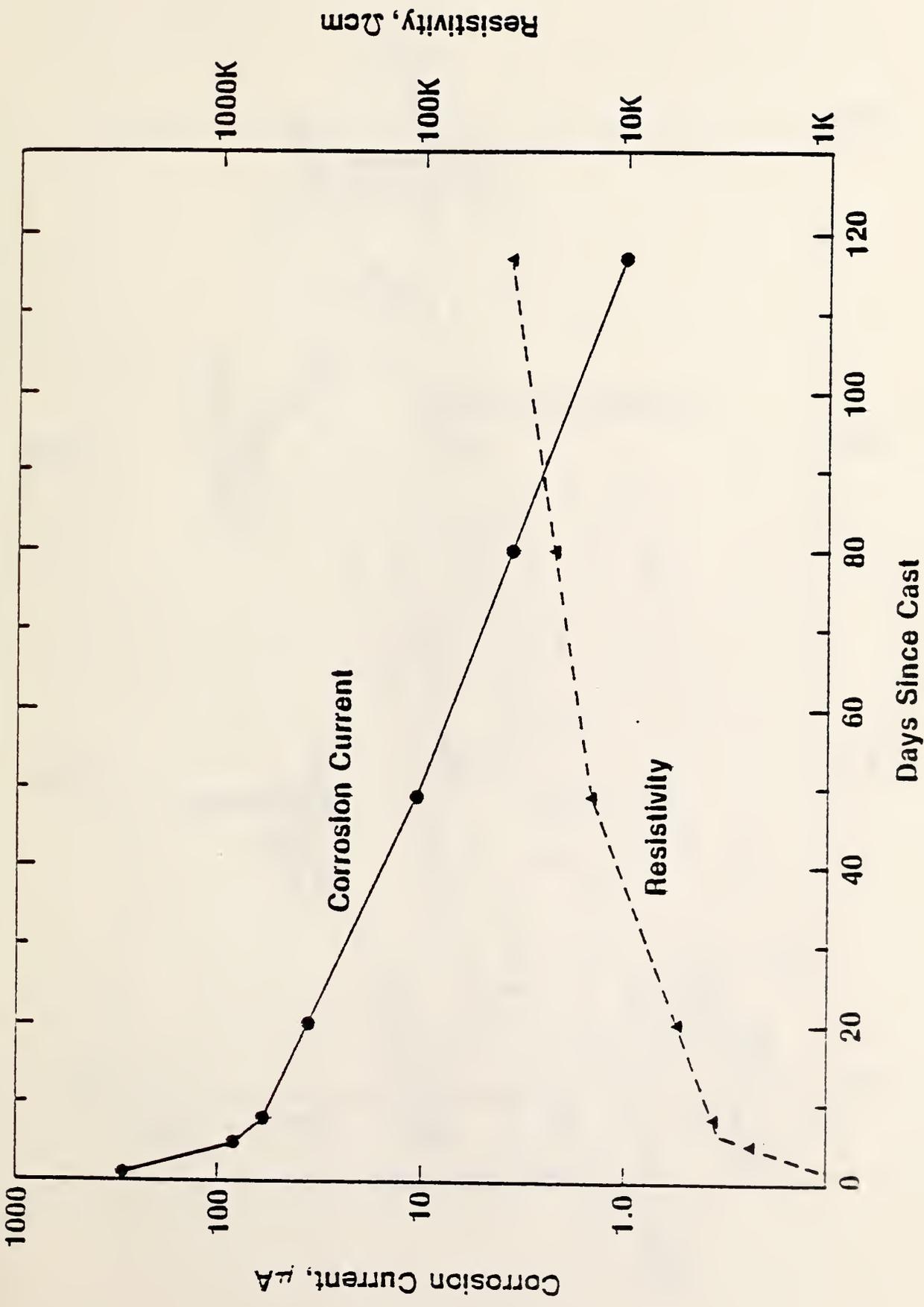


Figure 3

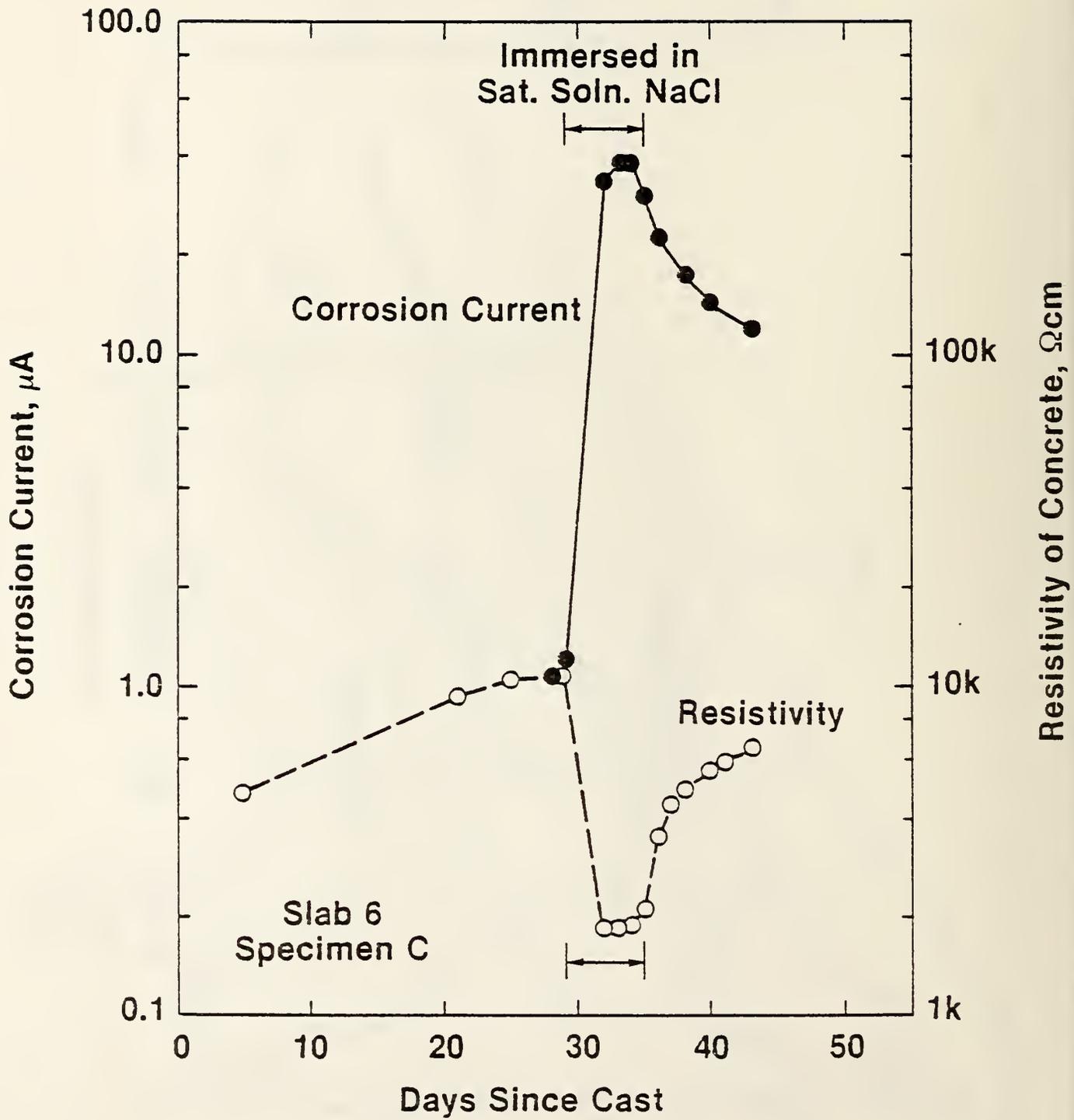


Figure 4

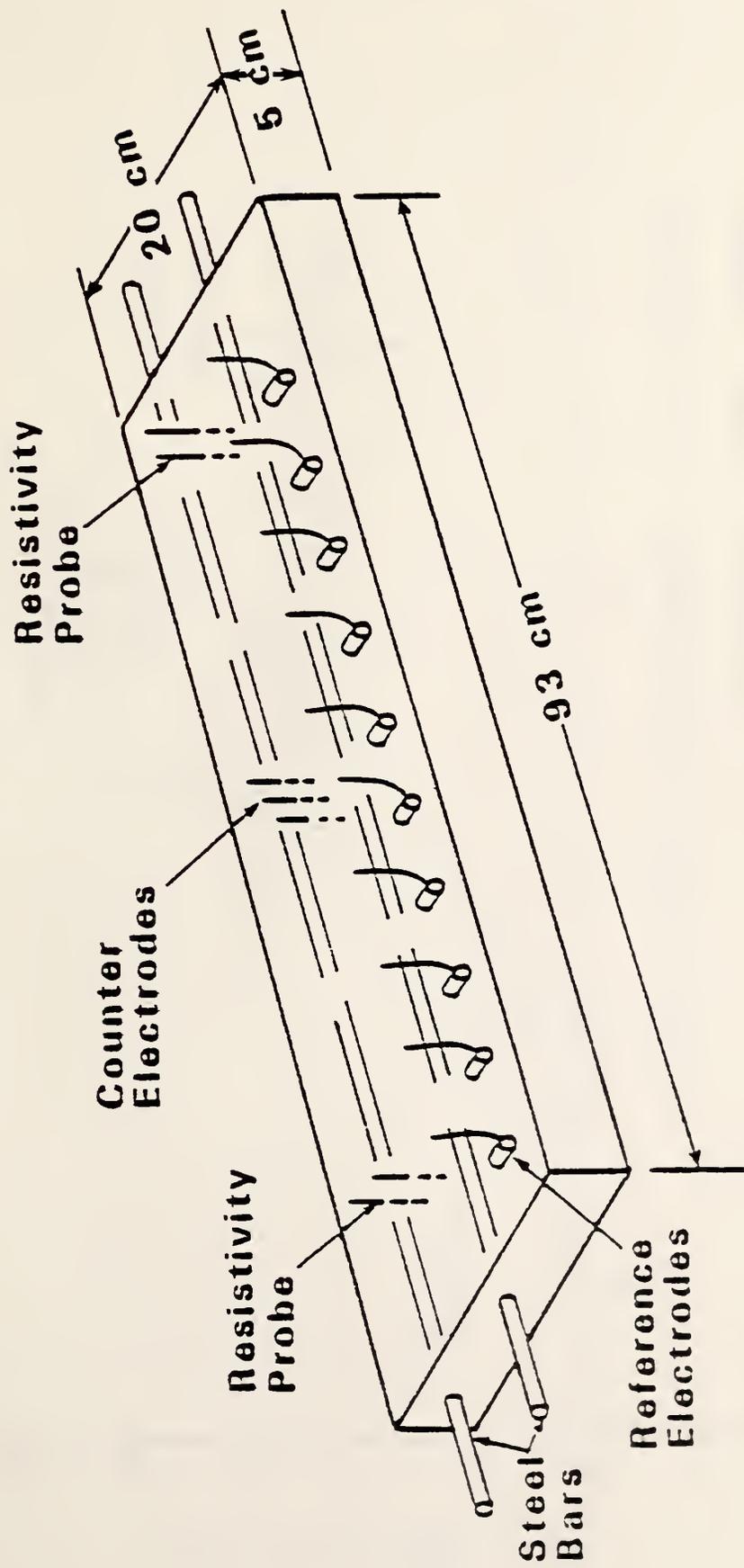


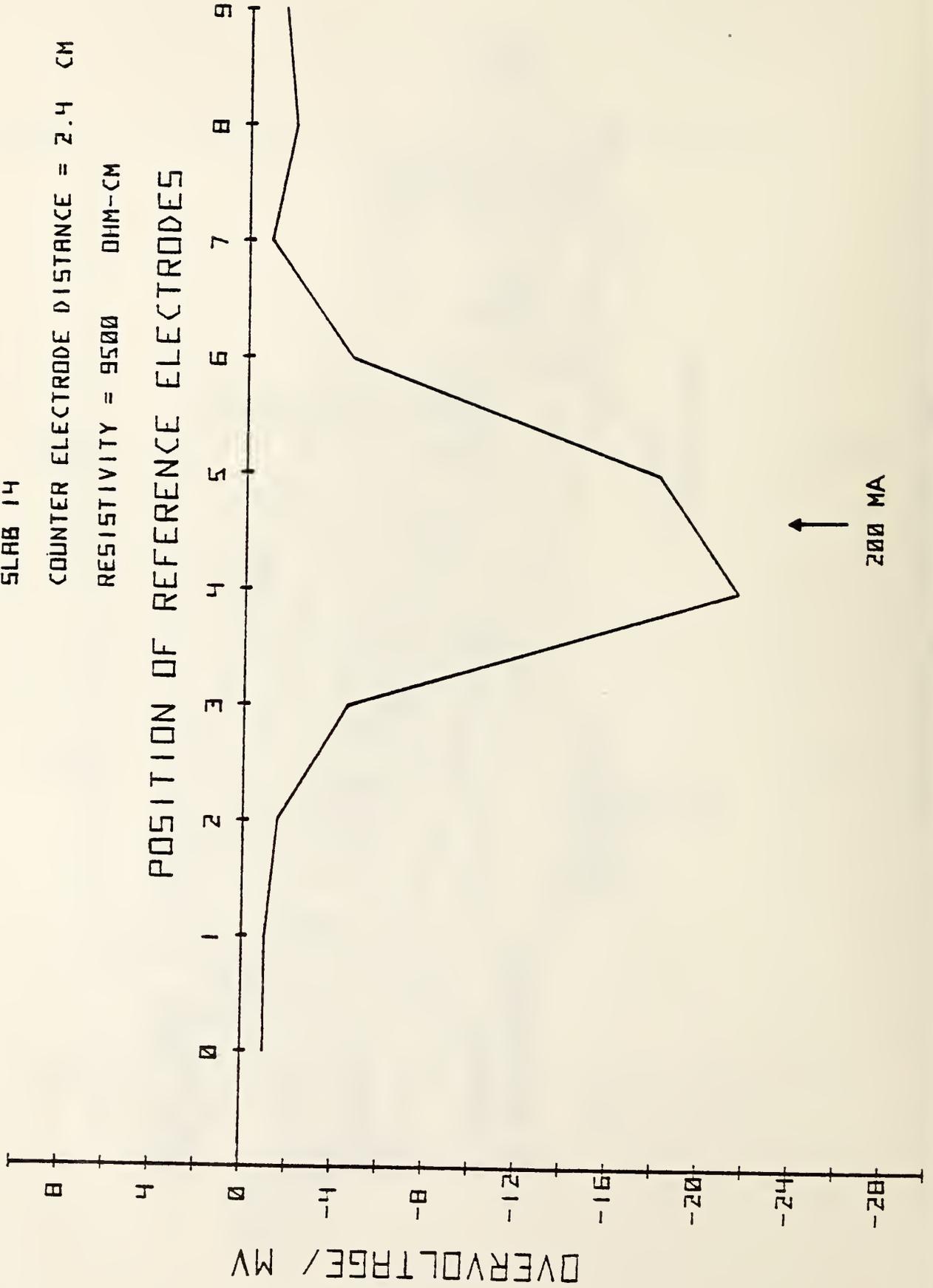
Figure 5

SLAB 14

COUNTER ELECTRODE DISTANCE = 2.4 CM

RESISTIVITY = 9500 OHM-CM

POSITION OF REFERENCE ELECTRODES



↑
200 MA

Figure 6

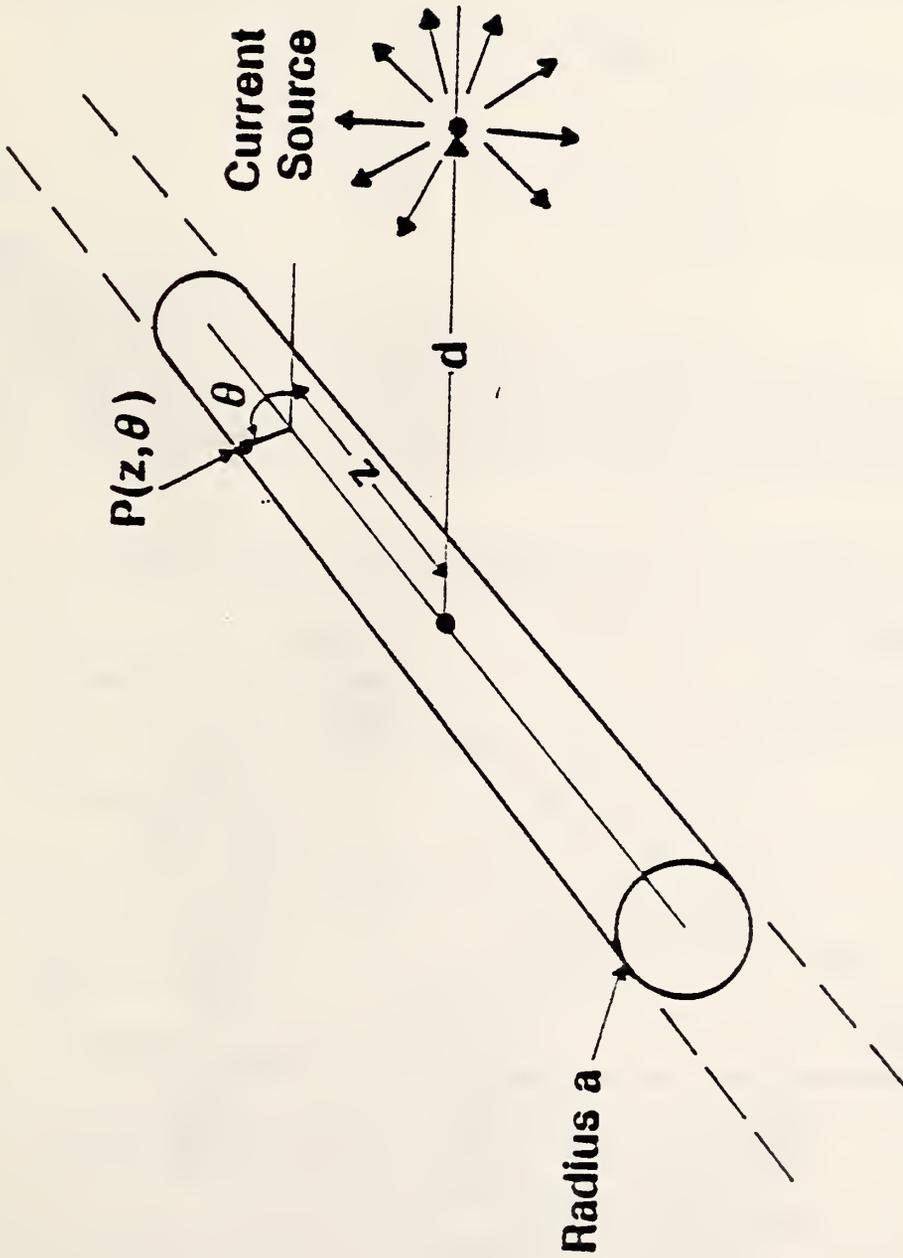
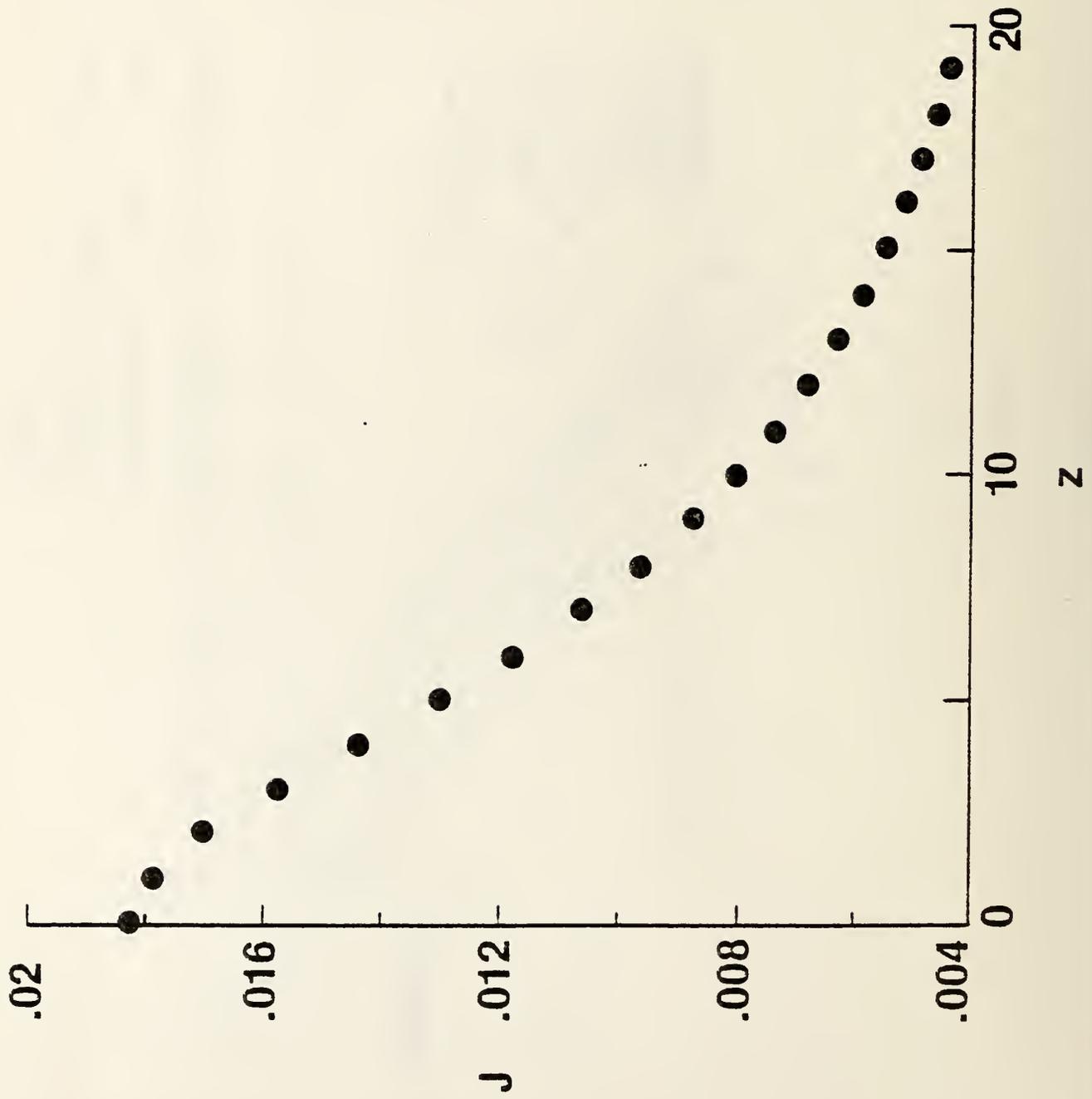


Figure 7



PANEL WIRING

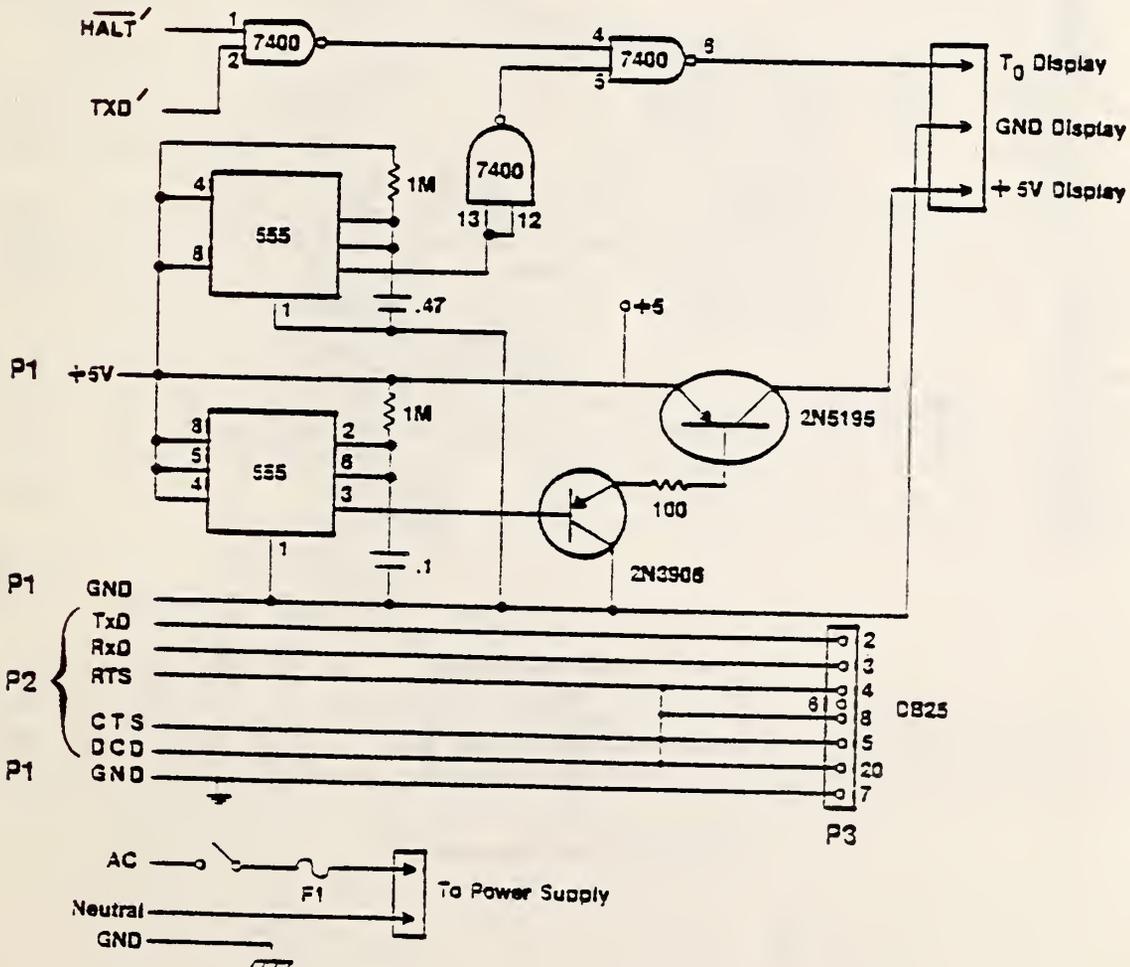
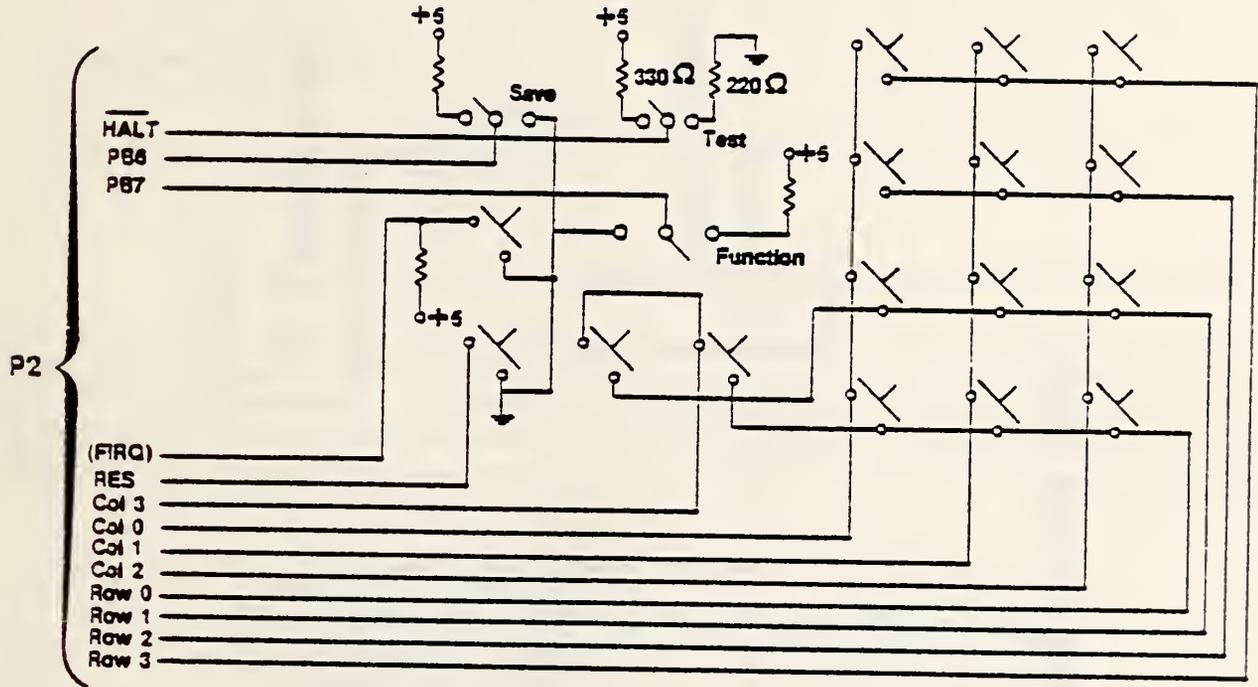


Figure 9

Modification to 1614 Module (10 Bit DAC)

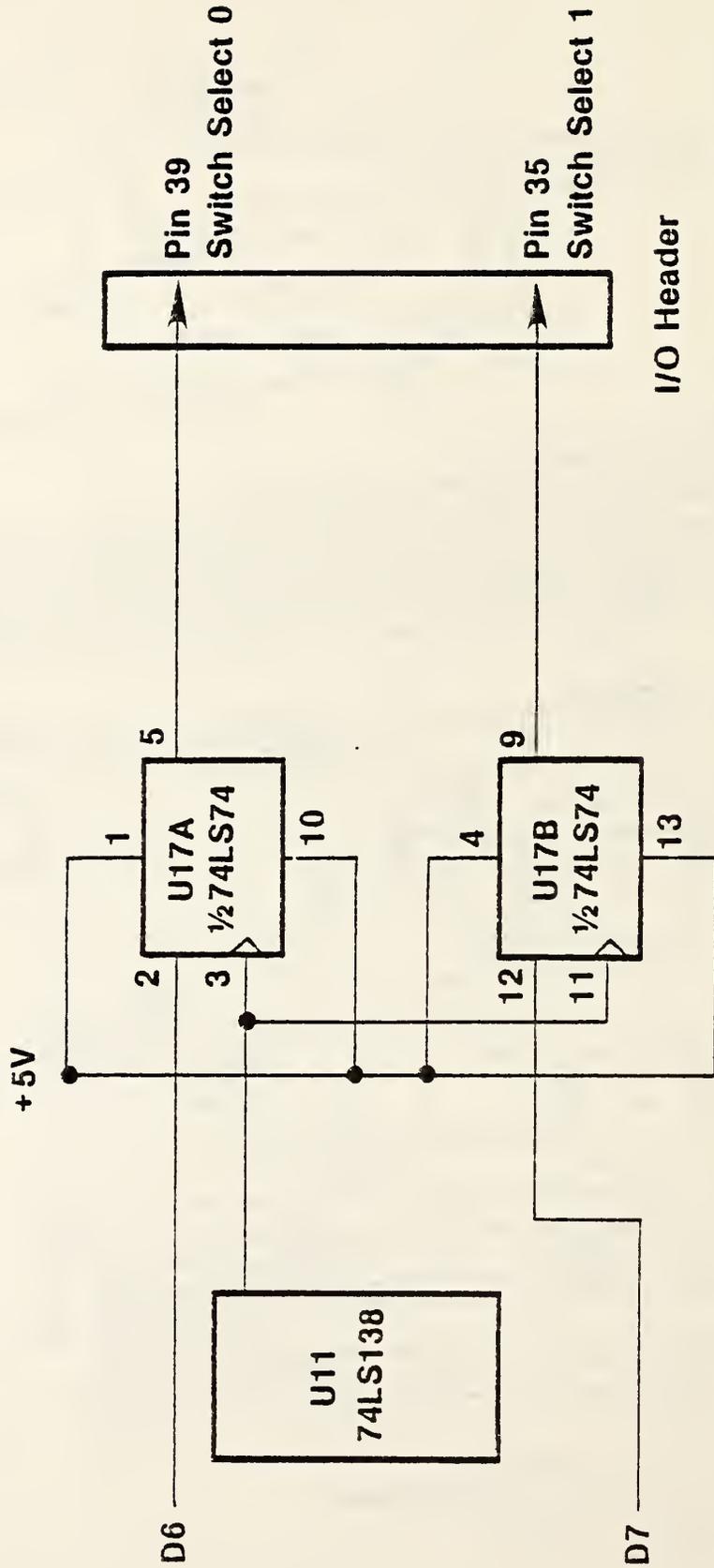


Figure 10

Keyboard Scanner Card

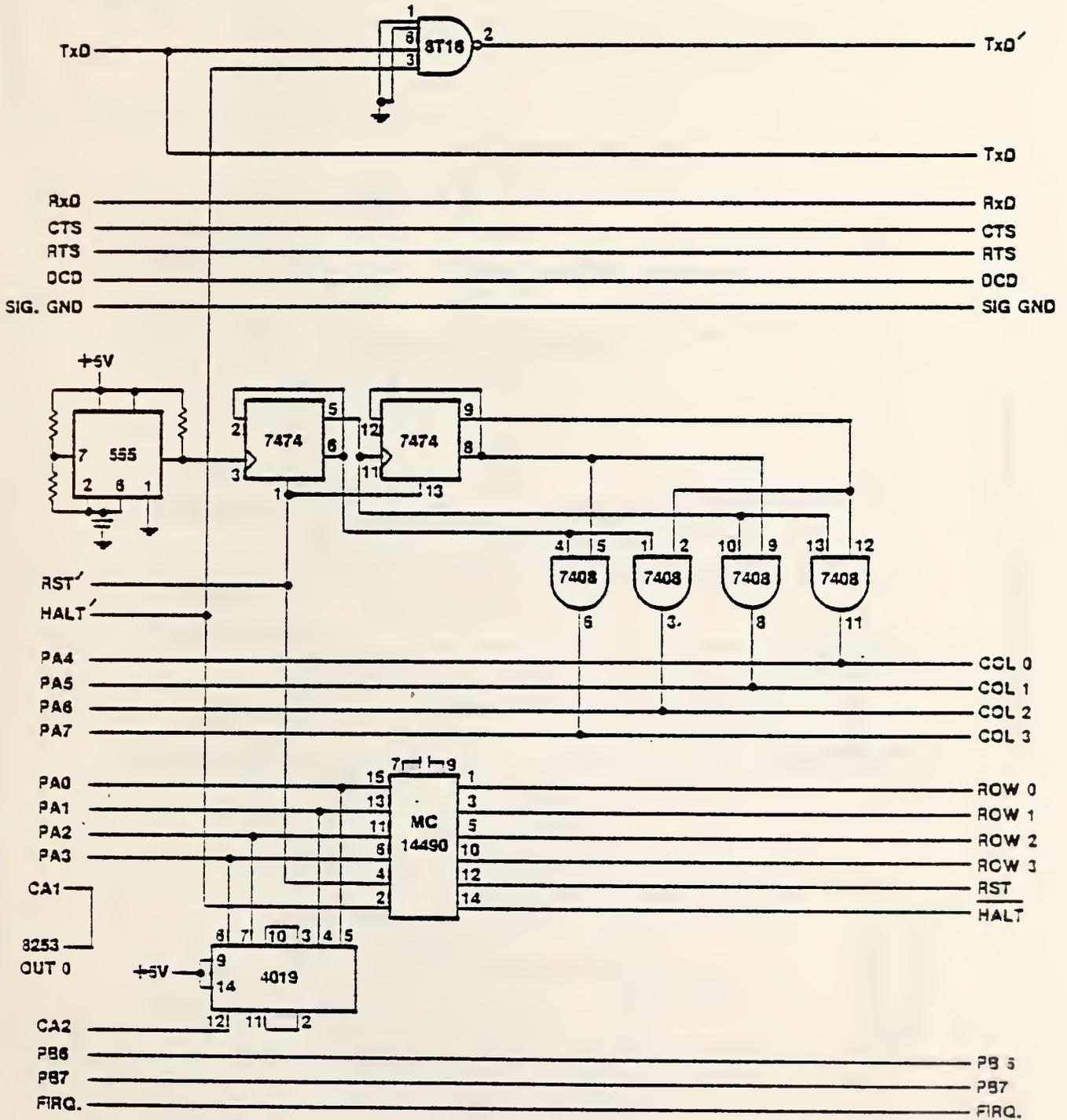
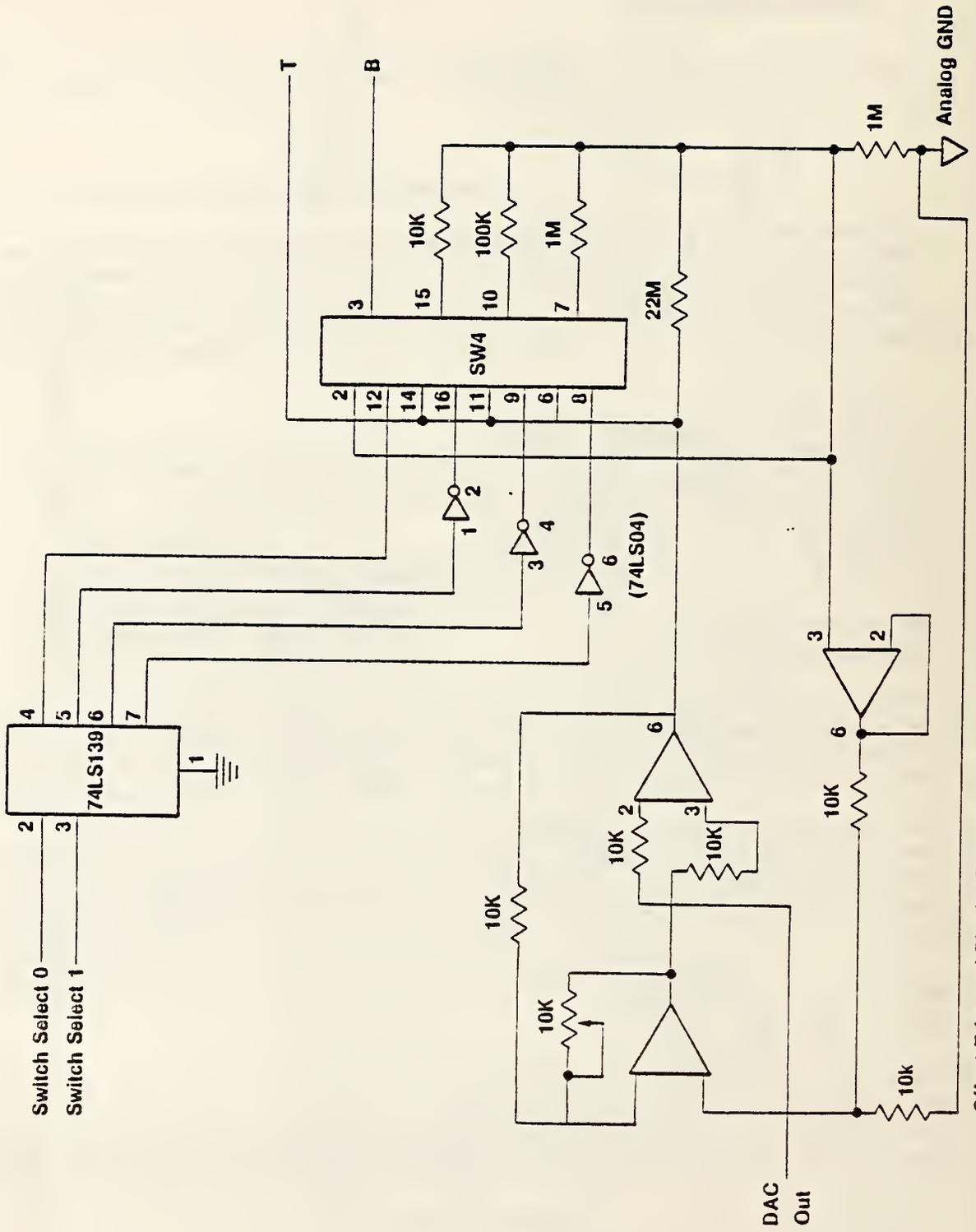


Figure 11

Voltage to Current Converter



Offset Trim and Bipolar Power Not Shown

Input Card

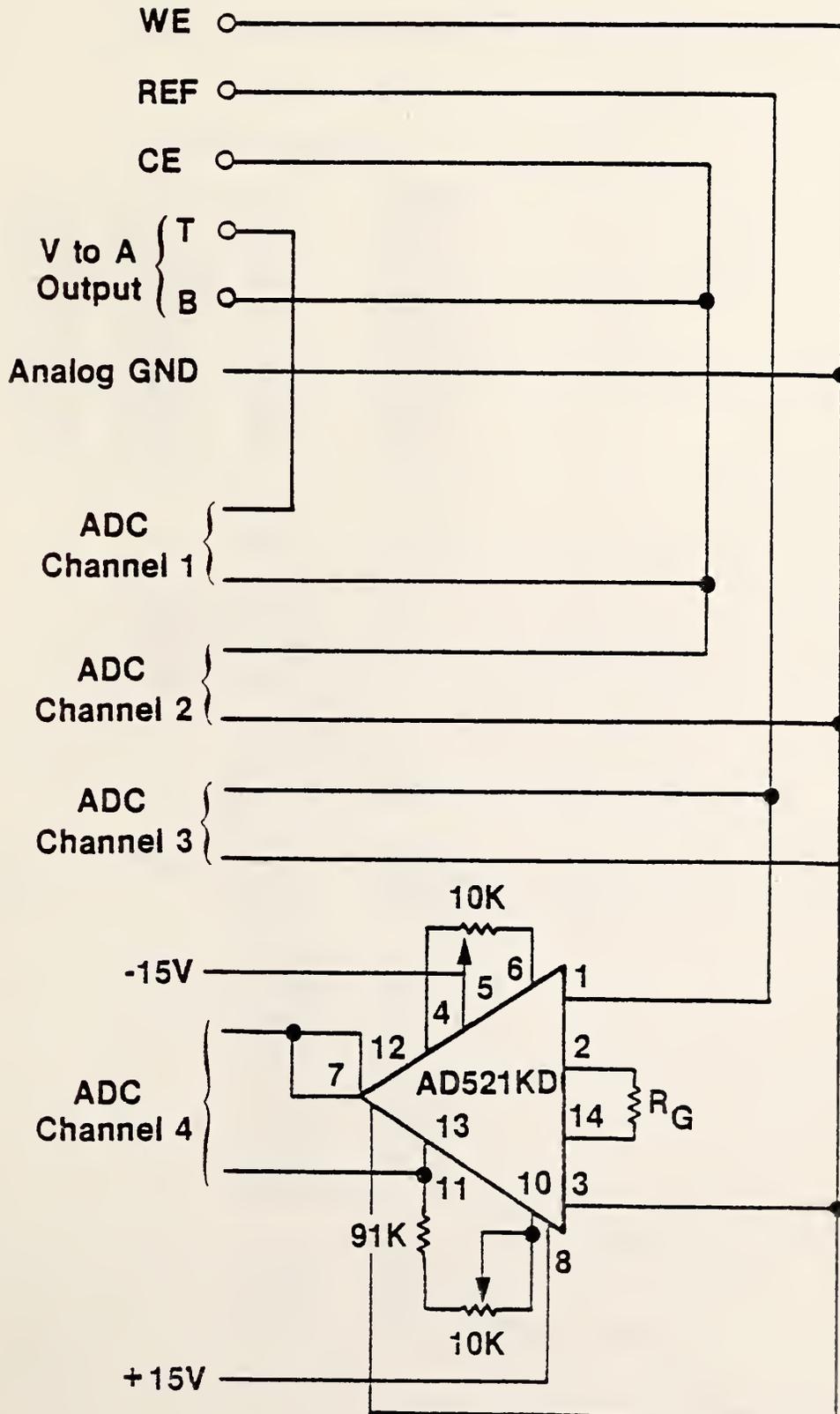


Figure 13

* BEGIN

* THIS ROUTINE ISSUES PROMPTS AND STORES CONSTANT
* DATA FOR THE PORTABLE INSTRUMENT

OPT EXP

* SYSTEM EQUATES

0800	BUFFER	EQU	\$0800
FECA	WFS	EQU	\$FECA
F9A3	GETDATA	EQU	\$F9A3
0743	STARTD	EQU	\$0743
070B	DATBUF	EQU	\$070B
FB9C	PACKS	EQU	\$FB9C
FA83	CVDTB	EQU	\$FA83
0731	RUNFLG	EQU	\$0731
FB6A	GETR	EQU	\$FB6A
F194	MEASUR	EQU	\$F194

0745 ORG \$0745

0745 RUNSET RMB 4

0749 TIMSET RMB 4

074D AREAST RMB 4

0751 WORK RMB 5

0007 SETDF \$07

F000 ORG \$F000

F000	0F	31	BEGIN	CLR	RUNFLG	
F002	BE	0800		LDX	#BUFFER	GET START OF BUFFER
F005	9F	0B		STX	DATBUF	SAVE IT

MSG	MACRO
	LBSR WFS
	FCB \$0D,\$0A
	FCC '&1'
	FCB \$0
	LDB ##&2
	LBSR GETDATA
	BEQ &0
	ENDM

F007 ID MSG "ID (15 CHAR,-MAX) = ", "10"

F007 17 0EC0 LBSR WFS

F00A 0D 0A FCB \$0D,\$0A

F00C 49 44 20 2B FCC 'ID (15 CHAR,-MAX) = '

F010 31 35 20 43

F014 4B 41 52 2E

F01B 2D 4D 41 5B

F01C 29 20 3D 20

F020	00		FCB	\$0	
F021	C6	10	LDB	##10	
F023	17	097D	LBSR	GETDATA	
F026	27	DF	BEQ	ID	
			ENDM		
F028		DATE	MSG	"DATE (DDMMYR) = ",7	
F028	17	0E9F	LBSR	WFS	
F02B	0D	0A	FCB	\$0D,\$0A	
F02D	44	41 54 45	FCC	'DATE (DDMMYR) = '	
F031	20	28 44 44			
F035	4D	4D 59 52			
F039	29	20 3D 20			
F03D	00		FCB	\$0	
F03E	C6	07	LDB	##7	
F040	17	0960	LBSR	GETDATA	
F043	27	E3	BEQ	DATE	
			ENDM		
F045		TIME	MSG	"TIME TO NEXT MEASUREMENT (MMSS)= ",5	
F045	17	0EB2	LBSR	WFS	
F04B	0D	0A	FCB	\$0D,\$0A	
F04A	54	49 4D 45	FCC	'TIME TO NEXT MEASUREMENT (MMSS)= '	
F04E	20	54 4F 20			
F052	4E	45 58 54			
F056	20	4D 45 41			
F05A	53	55 52 45			
F05E	4D	45 4E 54			
F062	20	28 4D 4D			
F066	53	53 29 3D			
F06A	20				
F06B	00		FCB	\$0	
F06C	C6	05	LDB	##5	
F06E	17	0932	LBSR	GETDATA	
F071	27	D2	BEQ	TIME	
			ENDM		
F073	9E	0B	LDX	DATBUF	POINT TO DATA
F075	34	20	PSHS	Y	SAVE Y
F077	30	1B	LEAX	-5,X	POINT TO MINUTES DATA
F079	17	00C0	LBSR	CUTIM	GO CONVERT TO BINARY
F07C	86	3C	LDA	#60	LOAD SEC/MIN
F07E	3D		MUL		MULTIPLY
F07F	DD	49	STD	TIMSET	
F081	9E	0B	LDX	DATBUF	POINT TO DATA, AGAIN
F083	30	1D	LEAX	-3,X	POINT TO SECONDS
F085	17	00B4	LBSR	CUTIM	CONVERT TO BINARY
F088	D3	49	ADDD	TIMSET	
F08A	DD	49	STD	TIMSET	
F08C	35	20	PULS	Y	
F08E		AREA	MSG	"AREA OF SAMPLE (0-65535 CM ²)= ",6	
F08E	17	0E39	LBSR	WFS	
F091	0D	0A	FCB	\$0D,\$0A	
F093	41	52 45 41	FCC	'AREA OF SAMPLE (0-65535 CM ²)= '	
F097	20	4F 46 20			
F09B	53	41 4D 50			
F09F	4C	45 20 28			
F0A3	30	2D 36 35			
F0A7	35	33 35 20			
F0AB	43	4D 5E 32			

F0AF	29	3D	20						
F0B2	00					FCB	\$0		
F0B3	C6	06				LDB	#\$6		
F0B5	17	08EB				LBSR	GETDATA		
F0BB	27	D4				BEQ	AREA		
						ENDM			
F0BA	9E	0B				LDX	DATBUF	POINT TO INPUT DATA	
F0BC	34	20				PSHS	Y	SAVE Y	
F0BE	8D	76				BSR	INSAU		
F0C0	DD	4D				STD	AREAST	SAVE BINARY AREA	
F0C2	35	20				PULS	Y		
F0C4				RUNS	MSG	"RUNS	COUNT (100 OR LESS)= "	,6	
F0C4	17	0E03			LBSR	WFS			
F0C7	0D	0A			FCB	\$0D,\$0A			
F0C9	52	55	4E	53	FCC	'RUNS COUNT (100 OR LESS)= '			
F0CD	20	43	4F	55					
F0D1	4E	54	20	2B					
F0D5	31	30	30	20					
F0D9	4F	52	20	4C					
F0DD	45	53	53	29					
F0E1	3D	20							
F0E3	00								
F0E3	00				FCB	\$0			
F0E4	C6	06			LDB	#\$6			
F0E6	17	08BA			LBSR	GETDATA			
F0E9	27	D9			BEQ	RUNS			
					ENDM				
F0EB	9E	0B			LDX	DATBUF	POINT TO DATA		
F0ED	34	20			PSHS	Y	SAVE Y		
F0EF	8D	45			BSR	INSAU			
F0F1	DD	45			STD	RUNSET	SAVE BINARY NUMBER OF RUNS		
F0F3	35	20			PULS	Y			
F0F5	BE	0B00		CRT000	LDX	#BUFFER	POINT TO START OF INPUT DATA		
F0F8	A6	80		CHARN	LDA	X+	GET CHAR		
F0FA	B1	0D			CMFA	#\$0D	IS IT A CR?		
F0FC	27	5C			BEQ	CG	IF SO, CHANGE IT		
F0FE	9C	0B		CNTCM	CPX	DATBUF	HAVE WE REACHED END?		
F100	26	F6			BNE	CHARN	IF NOT, GET ANOTHER CHAR.		
F102	8D	5B			BSR	DATSAU			
F104	CC	F194			LDD	#MEASUR	POINT TO MEASUREMENT ROUTINE		
F107	DD	31			STD	RUNFLG			
F109	17	0DBE			LBSR	WFS			
F10C	0D	0A			FCB	\$0D,\$0A			
F10E	50	52	45	53	FCC	'PRESS RUNWHEN READY FOR MEASUREMENT'			
F112	53	20	52	55					
F116	4E	20	57	4B					
F11A	45	4E	20	52					
F11E	45	41	44	59					
F122	20	46	4F	52					
F126	20	4D	45	41					
F12A	53	55	52	45					
F12E	4D	45	4E	54					
F132	00								
F132	00				FCB	00			
F133	16	0A34			LBSR	GETR			
F136	30	1A		INSAU	LEAX	-6,X			
F138	17	0948			LBSR	CUDTB	CONVERT TO BINARY		
F13B	39				RTS				

```

F13C 10BE 0751      CUTIM  LDY    #WORK
F140 C6 03          LDB    #3
F142 B6 30          LDA    #30
F144 A7 A0          THIRTY STA    Y+
F146 5A             DECB
F147 26 FB          BNE    THIRTY
F149 C6 02          LDB    #2
F14B A6 B0          SIXTY  LDA    X+      GET DATA
F14D A7 A0          STA    Y+      SAVE IT
F14F 5A             DECB
F150 26 F9          BNE    SIXTY
F152 1F 21          TFR    Y,X
F154 B0 1B          LEAX   -5,X
F156 17 092A        LBSR   CVDTB
F159 B9             RTS

F15A 4F             CG      CLRA
F15B A7 1F          STA    -1,X    REPLACE OR BY ZERO
F15D 20 9F          BRA    CNTCM

F15F 34 20          DATSAV PSHS   Y      SAVE Y
F161 109E 43        LDY    STARTD  GET CMOS MEMEORY START
F164 8E 0B00        LDX    #BUFFER POINT TO DATA
F167 DC 0B          LDD    DATBUF
F169 B2 0B00        SUBD   #BUFFER
F16C 47             ASRA    DIVIDE BY 4
F16D 56             RORB
F16E 47             ASRA
F16F 56             RORB
F170 17 0A29        LBSR   PACKS
F173 109F 43        STY    STARTD  SAVE NEXT CMOS DATA ADDRESS
F176 9E 0B          LDX    DATBUF  POINT TO DATA INPUT AREA
F178 B5 A0          PULS   Y,PC    RESTORE Y,RETURN

END

```

0 ERROR(S) DETECTED

SYMBOL TABLE:

AREA	F0BE	AREAST	074D	BEGIN	F000	BUFFER	0B00	CG	F15A
CHARN	F0FB	CNTCM	F0FE	CRTO00	F0F5	CVDTB	FAB3	CUTIM	F13C
DATBUF	070B	DATE	F028	DATSAV	F15F	GETDAT	F9A3	GETR	FB6A
ID	F007	INSAV	F136	MEASUR	F194	PACKS	FB9C	RUNFLG	0731
RUNS	F0C4	RUNSET	0745	SIXTY	F14B	STARTD	0743	THIRTY	F144
TIME	F045	TIMSET	0749	WFS	FECA	WORK	0751		

* MEASUR

* THIS ROUTINE HANDLES THE MEASUREMENT SEQUENCE IN
* THE PORTABLE INSTRUMENT. THE MEASURED DATA IS
* STORED IN THE CMOS MEMORY AND THE ADDRESS UPDATED
* FOR LATER RETRIEVAL IF DESIRED.

* SYSTEM EQUATES

0700	INDEX	EQU	\$0700
0702	ADCVAL	EQU	\$0702
0704	CHNUM	EQU	\$0704
0705	SWNUM	EQU	\$0705
0706	DACVAL	EQU	\$0706
0708	DATBUF	EQU	\$0708
0733	RUNCNT	EQU	\$0733
0743	STARTD	EQU	\$0743
0745	RUNSET	EQU	\$0745
0749	TIMSET	EQU	\$0749
B004	SAUST1	EQU	\$B004
DE50	DDAC	EQU	\$DE50

0007 SETDF \$07

FB2F	CGTIME	EQU	\$FB2F
FB39	TIMCHK	EQU	\$FB39
FB52	CHSELT	EQU	\$FB52
FB67	SMSFLT	EQU	\$FB67
FB79	CONVRT	EQU	\$FB79
FB9D	INITDA	EQU	\$FB9D
FB80	SWNSET	EQU	\$FB80
FBBF	SWNZER	EQU	\$FBBF
FBCB	LDDAC	EQU	\$FBCB
FECA	WFS	EQU	\$FECA

0751 ORG \$0751

0751	WORK	RMB	5
0756	REUFLG	RMB	1
0757	DACINI	RMB	2
0759	OPNCRK	RMB	2
075B	DACADJ	RMB	2

F194 ORG \$F194

F194 17 0D33 MEASUR LBSR WFS OUTPUT MESSAGE

F197 0D 0A FCB \$0D,\$0A

F199 57 4F 52 4B FCC 'WORKING'

F19D 49 4E 47

F1A0 00 FCB \$00

F1A1 0F 33 CLR RUNCNT

F1A3 CC 01FF LDD #\$01FF CORRESPONDS TO ZERO OUT

F1A6 DD 57 STD DACINI SAVE INITIAL VALUE

F1A8 CC 0033 LDD #\$0033 CORRESPONDS TO 1/2 MICROAMP

F1AB DD	5B		STD	DACADJ	SAVE ADJUSTMENT VALUE
F1AD 9E	4B		LDX	STARTD	GET START OF CMOS MEMORY AREA
F1AF BF	B004		STX	SAVST1	SAVE START OF MEMORY AREA
F1B2 CC	000A	SELCH	LDD	#\$000A	
F1B5 ED	B4		STD	X	
F1B7 17	0675		LBSR	CGTIME	SET TIMER FOR 1 MSEC TIMEOUTS
F1BA B6	01		LDA	#\$01	SET A TO D FOR CE TO WE, I-OFF
F1BC 97	04		STA	CHNUM	
F1BE 17	0691		LBSR	CHSELT	SELECT CHANNEL
F1C1 17	06A3		LBSR	SMSELT	START SAMPLING MODE
F1C4 17	0672		LBSR	TIMCHK	WAIT FOR TIMEOUT
F1C7 17	06AF		LBSR	CONVRT	MEASURE
F1CA ED	B1		STD	X++	SAVE VOLTAGE, I-OFF ZERO
F1CC 0C	04		INC	CHNUM	
F1CE 17	06B1		LBSR	CHSELT	
F1D1 17	0693		LBSR	SMSELT	
F1D4 17	06A2		LBSR	CONVRT	GET OPEN CIRCUIT POTENTIAL
F1D7 B6	00		LDA	#\$00	
F1D9 97	04		STA	CHNUM	
F1DB 17	0674		LBSR	CHSELT	SET A TO D TO CURRENT CHANNEL
F1DE 17	0686		LBSR	SMSELT	SET TO SAMPLING MODE
F1E1 17	041C		LBSR	SETIO	GET ZERO CURRENT VALUES
F1E4 DC	5B	CURSET	LDD	DACADJ	GET ADJUSTMENT VALUE
F1E6 44			LSRA		HALVE IT
F1E7 56			RORB		
F1EB D3	57		ADD	DACINI	ADD INITIAL VALUE
		*		*****	
		*		ALTERNATE IS SUBTRACTION FOR	
		*		OTHER POLARITY	
		*		*****	
F1EA DD	06		STD	DACVAL	
F1EC 0C	33	NEXT	INC	RUNCNT	
F1EE 9F	51		STX	WORK	SAVE INDEX
F1F0 17	0646		LBSR	TIMCHK	WAIT FOR TIMEOUT
F1F3 17	06D5		LBSR	LDDAC	SET CURRENT
F1F6 17	06B7		LBSR	SWNSET	SET SWITCH
F1F9 17	0630		LBSR	TIMCHK	WAIT FOR ANOTHER TIMEOUT
F1FC 17	067A		LBSR	CONVRT	GET POTENTIAL DROP OVER RESISTOR
F1FF ED	B1		STD	X++	SAVE R DROP
F201 0C	04		INC	CHNUM	
F203 17	064C		LBSR	CHSELT	
F206 17	065E		LBSR	SMSELT	SET TO READ CE TO WE POTENTIAL
F209 17	066D		LBSR	CONVRT	GET IT
F20C ED	B1		STD	X++	SAVE CE TO WE, I-ON
F20E 0C	04		INC	CHNUM	
F210 17	063F		LBSR	CHSELT	
F213 17	0651		LBSR	SMSELT	
F216 17	0620		LBSR	TIMCHK	
F219 17	0447		LBSR	SWZERO	TURN OFF CURRENT
F21C 17	065A		LBSR	CONVRT	GET WE-REF, I-OFF
F21F ED	B1		STD	X++	SAVE IT
F221 0A	04		DEC	CHNUM	POINT TO CE TO WE
F223 17	062C		LBSR	CHSELT	
F226 17	0629		LBSR	CHSELT	

F229	17	064D		LBSR	CONVRT	GET WE TO CE CURRENT OFF
F22C	ED	B1		STD	X++	SAVE IT
F22E	BF	B004		STX	SAVST1	SAVE NEXT DATA BLOCK ADDRESS
F231	0F	04		CLR	CHNUM	
F233	17	061C		LBSR	CHSELT	
F236	17	062E		LBSR	SMSFLT	SELECT CURRENT READ, AGAIN
F239	0D	56		TST	REVFLG	HAVE WE FOUND RANGE?
F23B	2B	06		BMI	RDONE	YES, THEN CALCULATE PARAMETERS
F23D	8D	3B		BSR	CALCI	DO CHECK FOR APPROPRIATE RANGES
F23F	9E	51		LDX	WORK	RESET INDEX
F241	30	A9		BRA	NEXT	
F243	DC	45	RDONE	LDD	RUNSET	GET # OF RUNS TO BE PERFORMED
F245	1027	008D		LBEQ	CALCII	IF ZERO GO CALCULATE
F249	D0	33		SUBB	RUNCNT	
F24B	102F	0087		LBLE	CALCII	IF DONE, DO FINAL CALCULATIONS
F24E	0F	4B		CLR	TIMSET+2	
F251	0F	4C		CLR	TIMSET+3	
F253	CC	2580		LDD	#\$2580	
F256	ED	B4		STD	X	SET TIMEOUT FOR ONE SEC
F258	17	05D4		LBSR	CGTIME	
F25B	17	05DB	TIMEOT	LBSR	TIMCHK	
F25E	DC	4B		LDD	TIMSET+2	
F260	C3	0001		ADD	#\$0001	
F263	DD	4B		STD	TIMSET+2	
F265	1093	49		CMFD	TIMSET	ARE WE DONE?
F268	27	02		BEQ	TIMUP	
F26A	20	EF		BRA	TIMEOT	
F26C	CC	000A	TIMUP	LDD	#\$000A	SET FOR 1 MILLISEC TIMEOUT
F26F	ED	B4		STD	X	
F271	17	05BB		LBSR	CGTIME	
F274	BE	B004	MORE	LDX	SAVST1	
F277	16	FF72		LBRA	NEXT	
F27A				ORG	0F27A	
F27A			CALCI	RMB	23	RESERVE AREA FOR NEXT PROGRAM
F291			TWOS	RMB	69	
F2D6			CALCII	RMB	2	ADDRESS OF CALCULATION PROGRAM
F600				ORG	0F600	
F600	B6	03	SETIO	LDA	#\$03	
F602	97	05		STA	SWNUM	POINT TO 5 MICROAMPERE FULL SCALE
F604	DC	57		LDD	DACINI	GET ZERO CURRENT EQUIVALENT
F606	DD	06		STD	DACVAL	SETUP TO OUTPUT IT
F608	DC	02	OPNSAV	LDD	ADCVL	GET OPEN CIRCUIT VOLTAGE
F60A	ED	B1		STD	X++	SAVE IT IN CMOS MEMORY
F60C	17	FCB2		LBSR	TWOS	
F60F	DD	59		STD	OPNCRK	
F611	17	0225		LBSR	TIMCHK	
F614	17	02B4		LBSR	LDDAC	SET FOR ZERO CURRENT
F617	17	0296		LBSR	SWNSRT	TURN ON ZERO CURRENT
F61A	17	021C		LBSR	TIMCHK	
F61D	0C	04		INC	CHNUM	POINT TO CE TO WE VOLTAGE
F61F	17	0230		LBSR	CHSELT	

```

F622 17 0242 -622 -14-14 LBSR SMSSELT
F625 17 0251 LBSR CONVURT GET APPLIED VOLTAGE-I ON
F62B DC 02 LDD ADCVAL RETRIEVE CE TO WE POTENTIAL
F62A ED B1 STD X++ SAVE IT
F62C B6 00 LDA #*00
F62E 97 04 STA CHNUM POINT TO CURRENT CHANNEL AGAIN
F630 17 021F LBSR CHSELT
F633 17 0231 LBSR SMSSELT
F636 17 0200 LBSR TIMCHK
F639 17 023D LBSR CONVURT GET DROP ACROSS R
F63C 17 0228 LBSR SMSSELT
F63F 17 027D LBSR SWNZER TURN OFF ZERO CURRENT
F642 DC 02 LDD ADCVAL RETRIEVE DROP ACROSS R
F644 ED B1 STD X++ SAVE IT
F646 B9 RTS

```

```

F647 DD 06 SETIO1 STD DACVAL SAVE ZERO CURRENT VALUE
F649 17 027F LBSR LDDAC SET CURRENT TO NEW ZERO
F64C 17 0261 LBSR SWNSET TURN ON CURRENT
F64F 17 01E7 LBSR TIMCHK
F652 17 0224 LBSR CONVURT GET NEW CURRENT ZERO
F655 17 0267 LBSR SWNZER TURN OFF SWITCH
F65B DC 02 LDD ADCVAL RETRIEVE VALUE
F65A ED 14 STD -12,X SAVE IT IN ZERO LOCATION
F65C 17 020B LBSR SMSSELT
F65F B9 RTS

```

```

F660 17 023A SWBEGN LBSR INITDA INITIALIZE DAC
F663 9F 00 SWZERO STX INDEX SAVE INDEX
F665 BE DE50 LDX #DDAC SET OUTPUT TO ZERO ROUTINE
F66B CC 8000 LDD #*B000
F66B ED B4 STD X
F66D E7 05 STB 5,X TURN OFF SWITCH
F66F 9E 00 LDX INDEX RESTORE INDEX
F671 B9 RTS

```

F672 END

0 ERROR(S) DETECTED

SYMBOL TABLE:

ADCVAL 0702	CALCI F27A	CALCII F2D6	CGTIME FB2F	CHNUM 0704
CHSELT FB52	CONVRT FB79	CURSET F1E4	DACADJ 075B	DACINI 0757
DACVAL 0706	DATABUF 070B	DDAC DE50	END F672	INDEX 0700
INITDA FB9D	LDDAC FBC8	MEASUR F194	MORE F274	NEXT F1EC
OPNCRK 0759	OPNSAV F608	RDONE F243	REVFLG 0756	RUNCNT 0733
RUNSET 0745	SAVST1 B004	SELCH F1B2	SETIO F600	SETIO1 F647
SMSSELT FB67	STARTD 0743	SWBEGN F660	SWNSET F8B0	SWNUM 0705
SWNZER F8BF	SWZERO F663	TIMCHK FB39	TIMEOT F25B	TIMSET 0749
TIMUP F26C	TWOS F291	WFS FECA	WORK 0751	

* CALCI

* THIS ROUTINE DOES CALCULATIONS FOR THE ADJUST-
* MENT OF THE CURRENT TO RESULT IN A FIXED REF TO
* WORKING ELECTRODE POTENTIAL

* SYSTEM EQUATES

0759 OPNCRK EQU \$0759
0733 RUNCNT EQU \$0733
075B DACADJ EQU \$075B
0706 DACVAL EQU \$0706
0705 SWNUM EQU \$0705
0756 REVFLG EQU \$0756
0757 DACINI EQU \$0757
FECA WFS EQU \$FECA
0731 RUNFLG EQU \$0731
FB6B GETR EQU \$FB6B
FC00 STARTCL EQU \$FC00
F647 SETIO1 EQU \$F647

COLD START ON ERROR

F27A ORG \$F27A

0007 SETDP \$07

F27A 0A 33 CALCI DEC RUNCNT REDUCE RUN COUNT TO REFLECT
* DATA NOT YET FOUND
F27C EC 1E LDD -2,X GET REF TO WE POTENTIAL
F27E A3 12 SUBD -14,X GET DIFFERENCE FROM OPEN CIRCUIT
F280 2B 19 BMI POLAR
F282 B4 0F TEST1 ANDA #\$0F CLEAR UPPER 4 BITS
F284 10B3 000A CMPD #\$000A IS THE DIFFERENCE 10 MV?
F288 2D 1B BLT ADJUST
F28A 96 56 LDA REVFLG
F28C BA F0 ORA #\$F0 SET FLAG TO INDICATE CURRENT FOUND
F28E 97 56 STA REVFLG
F290 39 RETURN RTS
F291 85 0B TWOS BITA #\$0B
F293 27 03 BEQ PLUS
F295 BA FB ORA #\$FB BIT 3--SET,SIGN EXTEND,ALL ONES
F297 39 RTS
F298 B4 07 PLUS ANDA #\$07 IF BIT 3 IS ZERO
F29A 39 RTS SIGN EXTEND ALL ZEROS, AND RETURN
F29B 8D 02 POLAR BSR NEGD GET TWO'S COMPLEMENT OF D
F29D 20 E3 BRA TEST1
F29F 43 NEGD COMA
F2A0 53 COMB
F2A1 C3 0001 ADDD #\$01
F2A4 39 RTS

```

F2A5 DC 06 ADJUST LDD DACVAL GET OLD CURRENT SET
F2A7 D3 5B ADDD DACADJ
F2A9 1083 03FF CMPD ##3FF HAVE WE REACHED FULL SCALE?
F2AD 2C 03 BGE RANGE
F2AF DD 06 CHANGE STD DACVAL
F2B1 39 RTS

F2B2 DC 57 RANGE LDD DACINI GET INITIAL VALUE
F2B4 0A 05 DEC SWNUM
F2B6 27 03 BEQ ERROR3
F2B8 16 03BC LBRA SETI01

F2BB 17 0C0C ERROR3 LBSR WFS
F2BE 0D 0A FCB $0D,$0A
F2C0 4F 55 54 20 FCC 'OUT OF RANGE'
F2C4 4F 46 20 52
F2C8 41 4E 47 45
F2CC 00 FCB $00
F2CD CC FC00 LDD #STARTCL
F2D0 DD 31 STD RUNFLG
F2D2 17 0B93 LBSR GETR

F2D6 ORG $F2D6

F2D6 CALCII RMB 2 ADDRESS OF NEXT ROUTINE

END

```

0 ERROR(S) DETECTED

SYMBOL TABLE:

ADJUST	F2A5	CALCI	F27A	CALCII	F2D6	CHANGE	F2AF	DACADJ	075B
DACINI	0757	DACVAL	0706	ERROR3	F2B8	GETR	FB68	NEGD	F29F
OPNCRK	0759	PLUS	F298	POLAR	F29B	RANGE	F2B2	RETURN	F290
REVFLG	0756	RUNCNT	0733	RUNFLG	0791	SETI01	F647	STARTC	FC00
SWNUM	0705	TEST1	F282	TWOS	F291	WFS	FECA		

0796			WSTORE	RMB	5	
079B			CNT	RMB	1	
		0007		SETDP	\$07	
F2D6				ORG	\$F2D6	
F2D6	CC	000A	CALCII	LDD	#\$0A	
F2D9	DD	B1		STD	TEN	SET SHIFT MULTIPLIER
F2DB	34	20		PSHS	Y	SAVE Y
F2DD	109E	43		LDY	STARTD	POINT TO ZERO DATA
F2E0	EC	B3		LDD	--X	GET MEASURED VALUE I-OFF
F2E2	A3	A1		SUBD	Y++	SUBTRACT ZERO VALUE
F2E4	2A	02		BPL	STORE1	
F2E6	8D	B7		BSR	NEGD	IF NEGATIVE, COMPLEMENT
F2E8	DD	5D	STORE1	STD	APVIOF	
F2EA	EC	B3		LDD	--X	GET OPEN CIRCUIT VALUE
F2EC	A3	A1		SUBD	Y++	SUBTRACT MEASURED VALUE
F2EE	2A	02		BPL	STORE2	
F2F0	8D	AD		BSR	NEGD	
F2F2	D0	5F	STORE2	STD	POTENT	SAVE IT
F2F4	27	7D		BEQ	ERROR5	
F2F6	EC	B3		LDD	--X	GET GET APPLIED VOLTAGE, I-ON
F2F8	A3	A1		SUBD	Y++	SUBTRACT CE TO WE, I-OFF
F2FA	2A	02		BPL	STORE3	
F2FC	8D	A1		BSR	NEGD	
F2FE	DD	61	STORE3	STD	APVION	
F300	27	71		BEQ	ERROR5	
F302	EC	B3		LDD	--X	GET DROP ACROSS RESISTOR
F304	A3	A1		SUBD	Y++	SUBTRACT ZERO CURRENT VALUE
F306	2A	02		BPL	STORE4	
F308	8D	95		BSR	NEGD	
F30A	DD	63	STORE4	STD	IRSW	
F30C	27	65		BEQ	ERROR5	
F30E	35	20		PULS	Y	
F310	9F	0B	RAPPAR	STX	DATEUF	SAVE INDEX
F312	0F	9B		CLR	CNT	
F314	0F	6B		CLR	EXPON	
F316	34	20		PSHS	Y	SAVE Y
F318	8E	0763		LDX	#IRSW	
F31B	108E	0761		LDY	#APVION	POINT TO VOLTAGE(CE TO WE)
F31F	17	025E		LBSR	SHIFT	
F322	DD	65		STD	RONEA	SAVE BINARY RESULT
F324	8E	076D		LDX	#RDAT1	POINT TO ASCII STORAGE AREA
F327	17	0787		LBSR	CVBTD	MAKE ASCII DATA AND STORE
F32A	35	20		PULS	Y	
F32C	8E	F3AC	CUR	LDX	#RTBL	POINT TO TABLE OF RESISTANCES
F32F	D6	05		LDB	SWNUM	GET WORKING SWITCH NUMBER
F331	3A			ABX		POINT TO VALUE
F332	A6	B4		LDA	X	
F334	27	56		BEQ	ERROR6	
F336	97	67		STA	RONEC	SAVE RESISTANCE
F338	8E	076D		LDX	#RDAT1	
F33B	17	00F6		LBSR	DECIMP	GO SET UP ASCII OUTPUT DATA
>F33E	16	006F		LBRA	CORRK	
F341	35	20	ERROR4	PULS	Y	

```

F343 17 0B84      LBSR      WFS
F346 0D 0A      FCB      $0D,$0A
F348 44 41 54 41  FCC      'DATA EXCEED ALLOWABLE POTENTIAL LIMITS!'
F34C 20 45 58 43
F350 45 45 44 20
F354 41 4C 4C 4F
F358 57 41 42 4C
F35C 45 20 50 4F
F360 54 45 4E 54
F364 49 41 4C 20
F368 4C 49 4D 49
F36C 54 53 21
F36F 00
F370 16 07F5      FCB      $00
                    LBRA      GETR

```

```

F373 17 0B54      ERROR5  LBSR      WFS
F376 0D 0A      FCB      $0D,$0A
F378 44 41 54 41  FCC      'DATA READS ZERO!'
F37C 20 52 45 41
F380 44 53 20 5A
F384 45 52 4F 21
F388 00
F389 16 07DC      FCB      $00
                    LBRA      GETR

```

```

F38C 17 0B3B      ERROR6  LBSR      WFS
F38F 0D 0A      FCB      $0D,$0A
F391 53 57 49 54  FCC      'SWITCH WAS SET TO ZERO!'
F395 43 48 20 57
F399 41 53 20 53
F39D 45 54 20 54
F3A1 4F 20 5A 45
F3A5 52 4F 21
F3A8 00
F3A9 16 07BC      FCB      $00
                    LBRA      GETR

```

```

F3AC 00      RTBL      FCB      $00      VALUES CORRESPONDING TO SWITCH
F3AD 04 05 06  FCB      $04,$05,$06 THESE ARE EXPONENTS

```

```

*****
*      FOR EPRI INSTRUMENT USE $02,$03,$04
*****

```

```

F3B0 86 00      CORRK   LDA      #$00      SET CONSTANT FOR CONVERSION
F3B2 97 68      STA      EXPON
F3B4 97 9B      STA      CNT
F3B6 04 20      PSHS     Y
F3B8 108E 075F   LDY      #POTENT
F3BC DC 5F      LDD      POTENT      GET VALUE OF REF TO WE
F3BE 10B3 0041   CMPD     #$0041
F3C2 102E FF7B   LBGT     ERROR4      GREATER THAN 65 MILLIVOLTS, ERROR
F3C6 8E 0763   LDX      #IRSW      POINT TO POTENTIAL ACROSS RESISTOR
F3C9 0C 9B      INC      CNT      SET TO MULTIPLY ANSWER BY TWO
F3CB 17 01B2   LBSR     SHIFT
F3CD 0A 68      DEC      EXPON      DIVIDE ANSWER BY TEN
F3D0 DD 69      STD      KONEA
F3D2 05 20      PULS     Y
F3D4 04 70      PSHS     X,Y,U
F3D6 0D 10      BSR      MLAREA      TIMES AREA - STORE ASCII DATA

```

F3DB	35	70		PULS	X,Y,U	RESTORE REGISTERS
F3DA	BE	8002		LDX	SAUST0	
F3DD	9F	00		STX	INDEX	
F3DF	BE	8004		LDX	SAUST1	GET FINAL ADDRESS OF DATA
F3E2	BF	8002		STX	SAUST0	START FOR SAVE CMOS MEMORY
F3E5	16	0082		LBRA	PUTDAT	
F3E8	BE	0769	MLAREA	LDX	#KONEA	POINT TO V/A DATA
F3EB	10BE	074D		LDY	#AREAST	POINT TO AREA DATA
F3EF	EC	A4		LDD	Y	GET AREA
F3F1	26	05		BNE	MLD	IF NON-ZERO GO
F3F3	CC	0001		LDD	#\$0001	IF AREA ZERO DEFAULT
F3F6	ED	A4		STD	Y	TO 1
F3F8	CE	0751	MLD	LDU	#WORK	POINT TO RESULT STORAGE LOCATION
F3FB	17	08C2		LBSR	MUL16	

* THE NEXT ROUTINE ROUNDS OFF DATA TO 16 BIT

F3FE	EC	C4	MLCHAR	LDD	U	FETCH STORED RESULT
F400	27	09		BEQ	CNTMC	IF NON-ZERO - ROUNDOFF NEEDED
F402	BD	16		BSR	ROUNDF	
F404	EC	42		LDD	2,U	GET DATA
F406	17	01AF		LBSR	SHIFTB	FINISH ROUNDOFF PROCEDURE
F409	ED	42		STD	2,U	SAVE RESULT
F40B	EC	42	CNTMC	LDD	2,U	GET ROUNDED DATA
F40D	DD	69		STD	KONEA	
F40F	BE	0777		LDX	#KDAT1	POINT TO ASCII STORAGE AREA
F412	17	069C		LBSR	CVBTD	MAKE ASCII AND STORE
F415	BE	0777		LDX	#KDAT1	
F418	20	1A		BRA	DECIMP	
F41A	84	FF	ROUNDF	ANDA	#\$FF	BYTE ZERO?
F41C	27	09		BEQ	BYTE2	
F41E	44			LSRA		SHIFT D RIGHT
F41F	56			RORB		
F420	17	01A0		LBSR	UPDATE	ELSE ADJUST LOWER HALF
F423	0C	9B		INC	CNT	
F425	20	F3	LOOPR	BRA	ROUNDF	DO NEXT BIT
F427	C4	FF	BYTE2	ANDB	#\$FF	IS BYTE ZERO?
F429	27	08		BEQ	ENDRND	GO, DONE
F42B	54			LSRB		ELSE SHIFT NEXT BIT
F42C	17	0194		LBSR	UPDATE	
F42F	0C	9B		INC	CNT	
F431	20	F4	LOOPB	BRA	BYTE2	
F433	39		ENDRND	RTS		
F434	96	67	DECIMP	LDA	RONEC	GET RESISTANCE EXPONENT
F436	9B	6B		ADDA	EXPON	ADJUST EXPONENT
F438	8B	04		ADDA	#\$04	POSITION ADJUST FOR DECIMAL POINT
F43A	97	6B		STA	EXPON	SAVE IT
F43C	81	0A		CMFA	#\$0A	IS EXPONENT 10
F43E	27	0F		BEQ	TENEXP	
F440	80	0A		SUBA	#\$0A	IS EXPONENT >10
F442	2B	06		BMI	SINGEX	

F444	1F	B9	TFR	A,B	SAVE ONES DIGIT
F446	B6	01	LDA	##01	SET TENS
F44B	20	0B	BRA	DECDAT	
F44A	4F		SINGEX	CLRA	SET TENS TO ZERO
F44B	D6	6B	LDB	EXPON	GET ONES DIGIT
F44D	20	03	BRA	DECDAT	
F44F	5F		TENEXP	CLRB	SET ONES DIGIT TO ZERO
F450	B6	01	LDA	##01	SET TENS TO ONE
F452	BA	30	DECDAT	ORA	##30
F454	CA	30	ORB	##30	MAKE EXPONENT ASCII
F456	E7	07	STB	7,X	
F45B	A7	06	STA	6,X	
F45A	A6	B4	LDA	X	
F45C	A7	1F	STA	-1,X	
F45E	B6	2E	LDA	#'	PUT DECIMAL POINT IN DATA
F460	A7	B4	STA	X	
F462	B6	45	LDA	#'E	PUT EXPONENTIAL SIGN IN DATA
F464	A7	05	STA	5,X	
F466	39		RTS		
F46A			ORG	##F46A	
F46A			PUTDAT	RMB	2
F46A					STARTING ADDRESS OUTPUT DATA
F5B0			ORG	##F5B0	
F5B0	EC	A4	SHIFT	LDD	0,Y
F5B2	DD	90		STD	PRESTR
F5B4	34	20		PSHS	Y
F5B6	10BE	0790		LDY	##PRESTR
F5BA	9F	00		STX	INDEX
F5B0	8E	0781	SHIFT1	LDX	##TEN
F5BF	CE	0751		LDU	##WORK
F592	17	022B		LBSR	MUL16
F595	0A	6B		DEC	EXPON
F597	DC	51		LDD	WORK
F599	26	06		BNE	USERND
F59B	0C	53		LDD	WORK+2
F59D	ED	A4		STD	0,Y
F59F	20	EB		BRA	SHIFT1
F5A1	17	FE76	USERND	LBSR	ROUNDF
F5A4	35	20		PULS	Y
F5A6	DC	53	USEABL	LDD	WORK+2
F5AB	27	22		BEQ	ERROR7
F5AA	ED	A4		STD	0,Y
F5AC	9E	00		LDX	INDEX
F5AE	34	40	PROCES	PSHS	U
F5B0	CE	0796		LDU	##WSTORE
F5B3	17	010B		LBSR	DIV16
F5B6	35	40		PULS	U
F5BB	0D	9B	SHIFTB	TST	CNT
F5BA	27	06		BEQ	ENDPRO
F5BC	5B			ASLB	
F5BD	49			ROLA	
F5BE	0A	9B		DEC	CNT
					ELSE MULTIPLY ANSWER BY 2

F5C0 20	F6		BRA	SHIFTB	
F5C2 39		ENDPRO	RTS		RETURN
F5C3 06	53	UPDATE	ROR	WORK+2	SHIFT LOWER WORD
F5C5 06	54		ROR	WORK+3	
F5C7 24	02		BCC	BACK	
F5C9 0C	54		INC	WORK+3	IF BIT WAS SET ADJUST LAST BIT
F5CB 39		BACK	RTS		
F5CC 35	20	ERROR7	PULS	Y	
F5CE 16	FDA2		LBRA	ERROR5	

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

APVIOF 075D	APVION 0761	AREAST 074D	BACK F5CB	BYTE2 F427
CALCII F2D6	CNT 079B	CNTMC F40B	CORRK F3B0	CVBTD FAB1
CVR F32C	DATEUF 070B	DECDAT F452	DECIMP F434	DIV16 F77E
ENDPRO F5C2	ENDRND F433	ERROR4 F341	ERROR5 F373	ERROR6 F38C
ERROR7 F5CC	EXPON 0768	GETR FB6B	INDEX 0700	IRSW 0763
KDAT0 0776	KDAT1 0777	KDAT6 077F	KONEA 0769	KTHREE 076B
LOOP8 F431	LOPR F425	MLAREA F3EB	MLCHAR F3FE	MLD F3FB
MUL16 F7C0	NEGD F29F	OPNCRK 0759	POTENT 075F	PRESTR 0790
PROCF3 F5AE	PUTDAT F46A	RAPPAR F310	RDAT0 076C	RDAT1 076D
RONEA 0765	RONEC 0767	ROUNDF F41A	RTBL F3AC	SAVST0 B002
SAVST1 B004	SHIFT F580	SHIFT1 F58C	SHIFTB F5BB	SINGEX F44A
STARTD 0743	STORE1 F2EB	STORE2 F2F2	STORE3 F2FE	STORE4 F30A
SWNUM 0705	TEN 07B1	TENEXP F44F	UPDATE F5C3	USEABL F5A6
USERND F5A1	WFS FECA	WORK 0751	WSTORE 0796	

* PUTDATA

* THIS ROUTINE OUTPUTS THE FINAL RESULTS TO THE
* DISPLAY. IT THEN PROMPTS FOR CMOS MEMORY SAVE,
* AND THEN FOR CONTINUATION. IF NOTHING FURTHER
* IS DESIRED, IT GOES INTO AN ENDLESS WAIT LOOP
* UNTIL POWER DOWN.

* SYSTEM EQUATES

0700 INDEX EQU \$0700
0B00 BUFFER EQU \$0B00
076C RDATA EQU \$076C
0776 KDATA EQU \$0776
DE20 ACIA EQU \$DE20
0756 REVFLG EQU \$0756
070B DATBUF EQU \$070B
0748 STARTD EQU \$0748

DE28 KEYPAD EQU \$DE28
F949 KBINCH EQU \$F949
FC00 STARTCL EQU \$FC00
FB7D PGMSAV EQU \$FB7D
FBCC LINFAS EQU \$FBCC
FECA WFS EQU \$FECA
FF0B WRC EQU \$FF0B
F2D6 CALCII EQU \$F2D6

0007 SETDF \$07

F46A ORG \$F46A

F46A 0D 56 PUTDAT TST REVFLG IS THIS FIRST OUTPUT POINT?
F46C 26 02 BNE HEADER IF SET, OUTPUT HEADER
F46E 20 22 BRA ROUT ELSE OUTPUT NEXT DATA POINT

F470 0F 56 HEADER CLR REVFLG
F472 17 00C5 LBSR CRLF
F475 8E 0B00 LDX #BUFFER POINT TO HEADER DATA

F47B C6 0F LDB #15 OUTPUT ID
F47A 108E DE20 LDY #ACIA
F47E 17 00C4 LBSR OUTDAT
F481 A6 B0 LDA X+ INCREMENT X, CHECK FOR LAST CHAR.
F483 1026 00D8 LBNE ERROR7

F487 17 00C4 OUTSS LBSR OUT4S
F48A C6 06 LDR #6
F48C 17 00B6 LBSR OUTDAT OUTPUT DATE
F48F 17 009C LBSR CHARIN WAIT FOR CHARACTER

F492	17	00A5	ROUT	LBSR	CRLF	
F495	17	0A32		LBSR	WFS	
F498	52	27 20 3D		FCC	"R" = ", \$00	
F49C	20	00				
F49E	8E	076C		LDX	#RDATA	POINT TO R'DATA
F4A1	C6	09		LDB	#9	
F4A3	17	009F		LBSR	OUTDAT	OUTPUT R'
F4A6	17	0A21		LBSR	WFS	
F4A9	20	4F 48 4D		FCC	' OHMS', \$00	
F4AD	53	00				
F4AF	8D	7D		BSR	CHARIN	WAIT FOR CHARACTER
F4B1	17	0086	KOUT	LBSR	CRLF	
F4B4	17	0A13		LBSR	WFS	
F4B7	4B	20 3D 20		FCC	'K = ', \$00	
F4BB	00					
F4BC	8E	0776		LDX	#KDATA	
F4BF	C6	09		LDB	#9	
F4C1	17	0081		LBSR	OUTDAT	OUTPUT K
F4C4	17	0A03		LBSR	WFS	
F4C7	20	4F 48 4D		FCC	' OHM X CM↑2 ', \$00	
F4CB	20	5B 20 43				
F4CF	4D	5E 32 20				
F4D3	20	00				
F4D5	8D	57		BSR	CHARIN	WAIT FOR CHARACTER
F4D7	9E	43		LDX	STARTD	GET BEGINNING OF FILE
F4D9	30	08		LEAX	B,X	OFFSET BY ZERO LOCATIONS
F4DB	9C	0B		CPX	DATBUF	HAVE WE REACHED END OF DATA
F4DD	27	05		BEQ	EXIT	
F4DF	9E	0B		LDX	DATBUF	ELSE, LOAD POINTER TO NEXT DATA
F4E1	16	FDF2		LBRA	CALCII	GO DO IT
F4E4	8D	54	EXIT	BSR	CRLF	
F4E6	17	09E1		LBSR	WFS	
F4E9	53	41 56 45		FCC	'SAVE DATA? YES = 1', \$00	
F4ED	20	44 41 54				
F4F1	41	3F 20 20				
F4F5	20	59 45 53				
F4F9	20	3D 20 31				
F4FD	00					
F4FE	8D	2E		BSR	CHARIN	
F500	C1	31		CMPB	##31	IS IT A ONE?
F502	27	31		BEQ	DSAVE	
F504	8D	34	ANOTHR	BSR	CRLF	
F506	17	09C1		LBSR	WFS	
F509	57	41 4E 54		FCC	'WANT ANOTHER RUN? YES = 1', \$00	
F50D	20	41 4E 4F				
F511	54	48 45 52				
F515	20	52 55 4E				
F519	3F	20 20 59				
F51D	45	53 20 3D				
F521	20	31 00				
F524	8D	0B		BSR	CHARIN	
F526	C1	31		CMPB	##31	
F52B	1027	06D4		LBEQ	STARTCL	
F52C	20	FE		BRA	*	THIS IS AN ENDLESS LOOP!

```

F52E B6 DE28 CHARIN LDA KEYPAD CLEAR KEYPAD
F531 17 0415 LBSR KBINCH
F534 39 RTS

F535 17 0645 DSAVE LBSR PGMSAV DISABLE CMOS MEMORY
F538 20 CA BRA ANOTHR

F53A 108E DE20 CRLF LDY #ACIA
F53E 17 0989 LBSR WFS
F541 0D 0A 00 FCB $0D,$0A,$00
F544 39 RTS

F545 A6 80 OUTDAT LDA X+
F547 17 09BE LBSR WRC OUTPUT CHAR.
F54A 5A DECB
F54B 26 FB BNE OUTDAT
F54D 39 RTS

F54E 9F 00 OUT4S STX INDEX
F550 108E DE20 LDY #ACIA
F554 17 0973 LBSR WFS
F557 20 20 20 20 FCB $20,$20,$20,$20,$00
F558 00
F55C 9E 00 LDX INDEX
F55E 39 RTS

F55F B6 3F ERROR7 LDA #'?
F561 17 09A4 LBSR WRC
F564 16 FF20 LBRA OUTSS

F567 END

```

0 ERROR(S) DETECTED

SYMBOL TABLE:

ACIA	DE20	ANOTHR	F504	BUFFER	0800	CALCII	F2D6	CHARIN	F52E
CRLF	F53A	DATBUF	070B	DSAVE	F535	END	F567	ERROR7	F55F
EXIT	F4E4	HEADER	F470	INDEX	0700	KBINCH	F949	KDAT0	0776
KEYPAD	DE2B	KOUT	F4B1	OUT4S	F54E	OUTDAT	F545	OUTSS	F487
PGMSAV	FB7D	PUTDAT	F46A	RDAT0	076C	REUFLG	0756	ROUT	F492
STARTC	FC00	STARTD	0743	UNPAKS	FBCC	WFS	FECA	WRC	FF0B

DIV151 F78E
DIV167 F7AD

DIV153 F799

DIV16 F77E

DIV163 F7A1

DIV165 F7AB

* MUL16

* THIS ROUTINE IS A 16 BIT BY 16 BIT MULTIPLY!
 * ONE NUMBER IS POINTED TO BY X, THE OTHER BY Y.
 * U POINTS TO STORAGE FOR THE RESULT. THIS
 * ROUTINE GENERATES A 32 BIT UNSIGNED RESULT.

* (A:B) X (C:D) = BDH:BDL
 * + BCH:BCL
 * + ADH:ADL
 * + ACH:ACL
 * -----

F7C0			ORG	\$F7C0	
F7C0	6F	C4	MUL16	CLR	0,U
F7C2	6F	41		CLR	1,U
F7C4	A6	01		LDA	1,X LEAST SIGN. BYTE NUMBER A
F7C6	E6	21		LDB	1,Y LEAST SIGN. BYTE NUMBER B
F7C8	3D			MUL	
F7C9	ED	42		STD	2,U SAVE RESULT
F7CB	A6	B4		LDA	0,X MOST SIGN. BYTE NUMBER A
F7CD	E6	21		LDB	1,Y LEAST SIGN. BYTE NUMBER B
F7CF	3D			MUL	
F7D0	E3	41		ADDD	1,U
F7D2	ED	41		STD	1,U
F7D4	24	02		BCC	AB1
F7D6	6C	C4		INC	0,U
F7D8	A6	01	AB1	LDA	1,X LEAST SIGN. BYTE NUMBER A
F7DA	E6	A4		LDB	0,Y MOST SIGN. BYTE NUMBER B
F7DC	3D			MUL	
F7DD	E3	41		ADDD	1,U
F7DF	ED	41		STD	1,U
F7E1	24	02		BCC	AB2
F7E3	6C	C4		INC	0,U
F7E5	A6	B4	AB2	LDA	0,X MOST SIGN. BYTE NUMBER A
F7E7	E6	A4		LDB	0,Y MOST SIGN. BYTE NUMBER B
F7E9	3D			MUL	
F7EA	E3	C4		ADDD	0,U
F7EC	ED	C4		STD	0,U
F7EE	39			RTS	
F7EF			END		

0 ERROR(S) DETECTED

SYMBOL TABLE:

F7D8 AB2 F7E5 END F7EF MUL16 F7C0

* ASTIMER

* THIS ROUTINE INITIALIZES THE TIMER IN THE
* MODULAS ONE SYSTEM, AND ALSO SETS TIMER
* PERIOD AND CHECKS FOR TIMEOUT OF TIMER 0.
* HANDLING OF TIMER ONE AND TWO CAN BE DONE
* IF DESIRED. SEE DATA SHEETS FOR TIMER AND
* MODULE 1140 MANUAL

* SYSTEM EQUATES

0034 CTRLT0 EQU \$34 INITIAL CONTROL STATE TIMER 0
0060 CTRLT1 EQU \$60 INITIAL CONTROL STATE TIMER 1
0099 CTRLT2 EQU \$99 INITIAL CONTROL STATE TIMER 2
0025 MSBT0 EQU \$25 MOST SIGNIFICANT BYTE COUNTER 0
00B0 LSBT0 EQU \$B0 LEAST SIGN. BYTE COUNTER 0
00FF LSBT1 EQU \$FF LEAST SIGN. BYTE COUNTER 1
0010 MSBT2 EQU \$10 MOST SIGN. BYTE COUNTER 2

* ADDRESSES

DE2C CT0 EQU \$DE2C COUNTER 0 ADDRESS
DE2D CT1 EQU \$DE2D COUNTER 1
DE2E CT2 EQU \$DE2E COUNTER 2
DE2F TIMER EQU \$DE2F CONTROL WORD FOR PROGRAMMING
DE29 CRA EQU \$DE29 PIA CONTROL REGISTER A
DE2B KPD EQU \$DE2B DATA REGISTER A--KEYPAD

* INITIALIZATION

FB00 ORG \$FB00
FB00 B6 34 INTIME LDA #CTRLT0 RESET TIMERS
FB02 B7 DE2F STA TIMER
FB05 B6 60 LDA #CTRLT1
FB07 B7 DE2F STA TIMER
FB0A B6 99 LDA #CTRLT2
FB0C B7 DE2F STA TIMER
FB0F B6 B0 LDA #LSBT0 SET INITIAL VALUES
FB11 B7 DE2C STA CT0
FB14 B6 25 LDA #MSBT0
FB16 B7 DE2C STA CT0
FB19 B6 FF LDA #LSBT1
FB1B B7 DE2D STA CT1
FB1E B6 10 LDA #MSBT2
FB20 B7 DE2E STA CT2
FB23 B9 RTS

* WHEN THE TIMER IS READ, IT INDICATES THE
 * NUMBER OF CLOCK PERIODS ELAPSED SINCE THE
 * LAST INTERRUPT (TIMEOUT) WAS GENERATED.
 * HERE, THE TIMER HAS BEEN INITIALIZED TO
 * GENERATE A TIMEOUT PULSE EVERY SECOND.
 * THE INPUT CLOCK IS A 9600 HERTZ PULSE INPUT
 * FROM THE BAUD RATE GENERATOR, AND THE TIMEOUT
 * APPEARS AT CA1 OF THE PIA.

* TO CHANGE THE TIMER PERIOD, THE COUNTER IS
 * LOADED WITH A NEW VALUE. THIS NEW COUNT
 * IS EFFECTIVE AFTER THE NEXT TIMEOUT PERIOD.

* READ TIMER--A AND B REGISTERS DESTROYED

FB24	4F		RDTIME	CLRA		
FB25	B7	DE2F		STA	TIMER	LATCH COUNTER 0
FB28	F6	DE2C		LDB	CT0	GET LSB OF COUNT
FB2B	B6	DE2C		LDA	CT0	GET MSB OF COUNT
FB2E	39			RTS		

* CHANGE TIMER PERIOD--A DESTROYED
 * X CONTAINS LOCATION
 * OF NEW VALUE

FB2F	A6	01	CGTIME	LDA	1,X	GET LSB OF NEW VALUE
FB31	B7	DE2C		STA	CT0	
FB34	A6	B4		LDA	X	GET MSB OF NEW VALUE
FB36	B7	DE2C		STA	CT0	COUNTER 0 NOW CONTAINS NEW PERIOD

FB39	B6	DE29	TIMCHK	LDA	CRA	CHECK FOR TIME OUT
FB3C	48			ASLA		
FB3D	24	FA		BCC	TIMCHK	
FB3F	B6	DE2B		LDA	KPD	CLEAR IRQ
FB42	39			RTS		TIMER NOW OPERATING AT NEW PERIOD

* TIMCHK IS ALSO USED AS SUBROUTINE CALL
 * FOR TIMING NEEDS.

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

CGTIME	FB2F	CRA	DE29	CT0	DE2C	CT1	DE2D	CT2	DE2E
CTRLT0	0034	CTRLT1	0060	CTRLT2	0099	INTIME	FB00	KPD	DE2B
LSBT0	0080	LSBT1	00FF	MSBT0	0025	MSBT2	0010	RDTIME	FB24
TIMCHK	FB39	TIMER	DE2F						

* ASATOD

* THIS ROUTINE PROVIDES A UTILITY PROGRAM TO
 * OPERATE THE ADAPTIVE SYSTEMS MODULAS ONE
 * A TO D MODULE #1642.

* SYSTEM EQUATES

DE10 DADC EQU \$DE10 BASE ADDRESS OF 1642 MODULE = PIA

0700 ORG \$0700

0700 INDEX RMB 2 RESERVE TWO LOCATIONS FOR X TEMP
 0702 ADCVAL RMB 2 LOCATION FOR LATEST ADC VALUE
 0704 CHNUM RMB 1 STORAGE FOR CURRENT CHANNEL

FB43 ORG \$FB43

0007 SETDF \$07

* INITIALIZATION---ASSUMES RESET HAS OCCURRED

FB43 8E DE10 INITAD LDX #DADC GET ADDRESS OF PIA
 FB46 CC 34F0 LDD #\$34F0
 FB49 A7 01 STA 1,X SET A SIDE--ALL INPUT,CA2 OUTPUT
 FB4B E7 02 STB 2,X SET B SIDE--FB4-7 OUT,FB0-3 IN
 FB4D 86 3C LDA #\$3C
 FB4F A7 03 STA 3,X SET CR2--OUTPUT, IRQ'S MASKED
 FB51 39 RTS

* CHANNEL SELECTION

FB52 9F 00 CHSELT STX INDEX SAVE INDEX
 FB54 8E DE10 LDX #DADC GET BASE ADDRESS
 FB57 96 04 LDA CHNUM
 FB59 4B ASLA
 FB5A 4B ASLA
 FB5B 4B ASLA
 FB5C 4B ASLA
 FB5D A7 02 STA 2,X PUT IN CHANNEL SELECT
 FB5F C6 08 LDB #8 DO APPROX. 50 MICROSEC DELAY
 FB61 5A ADC1 DECB FOR OP AMP TO STABILIZE
 FB62 26 FD BNE ADC1
 FB64 9E 00 LDX INDEX RESTORE INDEX
 FB66 39 RTS

* SELECT SAMPLING MODE

FB67 9F 00 SMSFLT STX INDEX SAVE INDEX
 FB69 8E DE10 LDX #DADC GET BASE ADDRESS
 FB6C CC 343C LDD #\$343C
 FB6F A7 01 STA 1,X SET CA2-LO FOR A/D SAMPLING

```

FB71 12      NOP
FB72 12      NOP
FB73 12      NOP
FB74 E7 03   STB      3,X      RESET ADC
FB76 9E 00   LDX      INDEX    RESTORE INDEX
FB78 39      RTS

```

* A/D CONVERSION

```

FB79 9F 00   CONVRT STX      INDEX    SAVE INDEX
FB7B BE DE10  LDX      #DADC
FB7E CC 3C34  LDD      #s3C34
FB81 A7 01   STA      1,X      SET CA2-HI FOR HOLD MODE
FB83 B6 04   LDA      #$4
FB85 E7 03   STB      3,X      START ADC CONVERSION (CB2-LO)
FB87 E6 03   ADC3   LDB      3,X      CHECK FOR EOC
FB89 2B 03   BMI      ADC4    IF RECEIVED--READ VALUE
FB8B 4A      DECA
FB8C 26 F9   BNE      ADC3    IF NOT FOUND, LOOP
                          UNTIL LOOP COUNTER = 0

FB8E A6 02   ADC4   LDA      2,X      READ UPPER 4 BITS
FB90 BA F0   ORA      #$F0     MASK OUTPUT BITS
FB92 E6 B4   LDB      0,X      GET LOWER 8 BITS
FB94 40      NEGA     DATA IS COMPLEMENTARY OFFSET BINAR

```

```

FB95 50      NEGB     MUST BE NEGATED
FB96 B2 00   SBCA     #0       ADJUST OVERFLOW
FB98 DD 02   STD      ADCVAL  SAVE RESULT
FB9A 9E 00   LDX      INDEX    RESTORE INDEX
FB9C 39      RTS

```

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

```

ADC1   FB61   ADC3   FB87   ADC4   FB8E   ADCVAL 0702   CHNUM  0704
CHSELT FB52   CONVRT FB79   DADC   DE10   INDEX  0700   INITAD FB48
SMELT  FB67

```

* ASDTOA

* THIS ROUTINE PROVIDES A UTILITY PROGRAM TO
* OPERATE THE ADAPTIVE SYSTEMS MODULAS ONE
* D TO A MODULE #1614

OPT PAG

* SYSTEM EQUATES

DE50 DDAC EQU \$DE50 DAC BASE ADDRESS
DE55 DSWITC EQU \$DE55 ANALOG SWITCH SELECT ADDRESS
0700 INDEX EQU \$0700 TEMP STORAGE FOR INDEX

0705 ORG \$0705
0705 SWNUM RMB 1 STORAGE FOR LATEST SWITCH VALUE
0706 DACVAL RMB 2 STORAGE FOR LATEST INPUT VALUE
0708 DACOLD RMB 2 STORAGE FOR PREVIOUS INPUT VALUE

0007 SETDF \$07

F89D ORG \$F89D

* INITIALIZATION

F89D 8E DE50 INITDA LDX #DDAC GET BASE ADDRESS
F8A0 4F CLRA
F8A1 06 LDB #6 ZERO DAC'S AND TURN SWITCH OFF
F8A3 8D 05 BSR DACINZ
F8A5 06 0A LDB #10
F8A7 8E 0700 LDX #INDEX

F8AA A7 80 DACINZ STA X+
F8AC 5A DECB
F8AD 26 FB BNE DACINZ
F8AF 39 RTS

* TURN SWITCH ON

F8B0 9F 00 SWNSSET STX INDEX SAVE INDEX
F8B2 8E DE55 LDX #DSWITC POINT TO SWITCH SELECT
F8B5 96 05 LDA SWNUM GET SWITCH NUMBER
F8B7 46 RORA MOVE NUMBER TO BITS 6 AND 7
F8B8 46 RORA
F8B9 46 RORA
F8BA A7 84 STA X SEND TO SWITCH SELECT
F8BC 9E 00 LDX INDEX RESTORE INDEX
F8BE 39 RTS

* TURN SWITCH OFF--ALTERNATE TO SWNSSET WITH 00
* DOES NOT CHANGE CONTENTS OF SWNUM

```

FB8F 9F 00 SWNZER STX INDEX SAVE INDEX
FB91 BE DE55 LDX #DSWITC
FB94 B6 00 LDA #$00
FB96 A7 84 STA 0,X
FB98 9E 00 LDX INDEX RESTORE INDEX
FB9A 89 RTS

```

* LOAD DAC VALUE

```

FB9B 9F 00 LDDAC STX INDEX SAVE INDEX
FB9D 8E DE50 LDX #DDAC POINT TO DAC 1
FB9F D6 06 LDB DACVAL GET DAC INPUT
FBA2 D7 0B STB DACOLD
FBA4 96 07 LDA DACVAL+1
FBA6 97 09 STA DACOLD+1
FBA8 54 LSRB SHIFT SO THAT 2 LO BITS ARE IN
FBA9 46 RORA BITS 6 AND 7 OF B AND 8 HI BITS
FBAB 56 RORB ARE IN A
FBAD 46 RORA
FBAD 56 RORB
FBAD ED 84 STD X OUTPUT VALUE TO DAC
FBDF 9E 00 LDX INDEX RESTORE INDEX
FBE1 89 RTS

```

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

DACINZ	FBAA	DACOLD	0708	DACVAL	0706	DDAC	DE50	DSWITC	DE55
INDEX	0700	INITDA	F89D	LDDAC	F8CB	SWNSET	FBB0	SWNUM	0705
SWNZER	FBBF								

* SAVECK

* THIS ROUTINE CHECKS FOR DISABLING OF THE
* CMOS MEMORY ON STARTUP, THE CONTENTS OF
* THIS CMOS MEMORY ARE SAVED BY DISABLING
* THE INPUT TO THE MEMORY, THIS IS DONE BY
* CLOSURE OF THE STORE KEY (ALTERNATE ACTION)
* PRIOR TO POWER-OFF OR WHENEVER DESIRED,
* ON RESET OR POWER-UP, THE UNIT WILL CHECK
* AND REQUEST RELEASE IF NEEDED, THAT IS THE
* FUNCTION OF THIS ROUTINE.

* SYSTEM EQUATES

DE2A ORB EQU \$DE2A ADDRESS OF DATA REG OF PIA
DE20 ACIA EQU \$DE20
FECA WFS EQU \$FECA ROUTINE TO WRITE STRING
070A SAVFLG EQU \$070A
0007 SETDP \$07
FBF0 ORG \$FBF0

* CHECK FOR SAVE AND REQUEST RELEASE
* ASSUMES INITIALIZATION COMPLETE!

FBF0 10BE DE20 SAVECK LDY #ACIA POINT TO COMMUNICATIONS REGISTER
FBF4 F6 DE2A LDB ORB GET PIA B DATA
FBF7 C4 40 ANDB #\$40 IS BIT 6 HI?
FBF9 27 04 BEQ CONT1 IF NOT HIGH, MEMORY HAS BEEN SAVED
FBFB 0F 0A CLR SAVFLG
FBFD 20 31 BRA CONT MEMORY AVAILABLE-CONTINUE
FBFF B6 FF CONT1 LDA #\$FF SET FLAG
F901 97 0A STA SAVFLG
F903 17 05C4 LBSR WFS REQUEST CLEARANCE OF DISABLE
F906 4D 45 4D 4F FCC 'MEMORY NOT AVAILABLE--UNSAVE!'
F90A 52 59 20 4E
F90E 4F 54 20 41
F912 56 41 49 4C
F916 41 42 4C 45
F91A 2D 2D 55 4E
F91E 53 41 56 45
F922 21
F923 00 FCB 0
F924 B6 04 CHECK LDA #\$4
F926 C6 40 CHECK1 LDB #\$40
F928 F5 DE2A BITB ORB
F92B 27 F7 BEQ CHECK
F92D 4A DECA
F92E 26 F6 BNE CHECK1 CHECK FOUR TIMES FOR COMPLETION
F930 17 0597 CONT LBSR WFS
F933 0D 0A FCB \$0D, \$0A

F935 52 45 41 44
F939 59
F93A 00
F93B 39

FCC 'READY'

FCB 0
RTS

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

ACIA	DE20	CHECK	F924	CHECK1	F926	CONT	F930	CONT1	FBFF
ORB	DE2A	SAVECK	FBF0	SAVFLG	070A	WFS	FECA		

* KPDCTL

* THIS ROUTINE CONTROLS THE OPERATION OF THE
* KEYPAD ON THE PORTABLE INSTRUMENT. THIS
* UTILITY IS CONCERNED ONLY WITH THE IMMEDIATE
* OPERATION OF THE KEYPAD AND THE ENTRY OF A
* SINGLE CHARACTER, AND ITS TRANSLATION INTO
* ASCII. OTHER ASPECTS OF KEYPAD USAGE ARE TO
* BE CONTROLLED BY THE CALLING ROUTINES.

* SYSTEM EQUATES

```
DE28 KEYPAD EQU $DE28 DRA OF PIA ON 1140 MODULE
0700 INDEX EQU $0700

0007 SETDP $07

F93C ORG $F93C
```

* INITIALIZATION--ASSUMES RESET

```
F93C 8E DE28 INITKP LDX #KEYPAD GET PIA BASE ADDRESS
F93F 86 14 LDA #$14 A SIDE-INPUT, IRQ'S MASKED
F941 A7 01 STA 1,X CA1 GOES LO, CA2 GOES HI
F943 CC 3F04 LDD #$3F04 B SIDE-2 IN, 6 OUT MASK IRQ'S
F946 ED 02 STD 2,X CB1 AND CB2 GO LO
F948 39 RTS
```

* READ KEYPAD--NO MATCH SHOWN BY ZERO BIT SET

```
F949 9F 00 KBINCH STX INDEX SAVE INDEX
F94B 34 40 PSHS U SAVE U
F94D CE DE28 LDU #KEYPAD
F950 B6 40 LDA #$40 SET MASK
F952 A5 41 CHARIN BITA 1,U DO WE HAVE A CHARACTER(CA2-HI)
F954 27 FC BEQ CHARIN LOOP, IF NOT
F956 A6 C4 LDA U ELSE, GET CHARACTER
F958 BE F96D LDX #KEYTBL

F95B A1 B1 KBIN1 CMPA X++
F95D 27 0A BEQ KBIN2
F95F BC F9B9 CPX KEYTBL+2B HAVE WE REACHED END OF TABLE?
F962 26 F7 BNE KBIN1
F964 5F CLR B CLR B
F965 9E 00 KBIN3 LDX INDEX SHOW NO MATCH FOUND!
F967 35 C0 PULS U,PC RESTORE U REGISTER, RETURN

F969 E6 1F KBIN2 LDB -1,X SHOW MATCH
F96B 20 FB BRA KBIN3
```

* TABLE TO CONVERT KEYPAD VALUE TO ASCII

```
F96D 11 0D KEYTBL FCB $11,$0D
```

F96F	12	33	FCB	\$12,\$33
F971	14	36	FCB	\$14,\$36
F973	18	39	FCB	\$18,\$39
F975	21	30	FCB	\$21,\$30
F977	22	32	FCB	\$22,\$32
F979	24	35	FCB	\$24,\$35
F97B	28	38	FCB	\$28,\$38
F97D	41	7F	FCB	\$41,\$7F
F97F	42	31	FCB	\$42,\$31
F981	44	34	FCB	\$44,\$34
F983	48	37	FCB	\$48,\$37
F985	81	4A	FCB	\$81,\$4A
F987	82	48	FCB	\$82,\$48

END

⊙ ERROR(S) DETECTED

SYMBOL TABLE:

CHARIN	F952	INDEX	0700	INITKF	F93C	KBIN1	F95B	KBIN2	F969
KBIN3	F965	KBINCH	F949	KEYPAD	DE28	KEYTBL	F96D		

* GETDATA

* THIS ROUTINE GETS A DATA STRING FROM THE
* KEYPAD OF THE PORTABLE INSTRUMENT. ENTRY
* REQUIRES THAT B CONTAIN THE NUMBER OF CHAR.
* REQUESTED AND X CONTAINS THE STARTING ADDRESS
* FOR STORAGE. THE ROUTINE FORMATS THE STRING
* SO THAT LEADING ZEROS ARE INSERTED TO FILL
* THE REQUESTED DATA BLOCK. STORAGE IS IN THE
* FORM OF ASCII CHARACTERS.

* INCLUDED IN THIS ROUTINE IS A SUBROUTINE TO
* ALLOW FOR APPROXIMATELY 100 MILLISEC PER
* CHARACTER

* SYSTEM EQUATES

F949	KBINCH	EQU	\$F949	INPUT CHARACTER FROM KEYPAD
FECA	WFS	EQU	\$FECA	STRING OUTPUT ROUTINE
0780	INDEX1	EQU	\$0780	TEMPORARY STORAGE FOR INDEX
FA0C	CMDADR	EQU	ERROR+\$A	
DE28	KEYPAD	EQU	\$DE28	
FF08	WRC	EQU	\$FF08	

070B		ORG	\$070B	
070B	DATBUF	RMB	2	STORAGE FOR LATEST BUFFER ADDRESS
070D	TCOUNT	RMB	1	STORAGE FOR WORKING COUNT
070E	TCHAR	RMB	1	STORAGE FOR WORKING CHARACTER
070F	TCHCNT	RMB	1	COUNTER FOR ACCESSES TO CHAR.
0710	TBUFFER	RMB	33	BUFFER AREA FOR STRING STORAGE
0731	RUNFLG	RMB	2	FLAG TO INDICATE RUN STATUS

0007 SETDF \$07

F9A3 ORG \$F9A3

F9A3	9E	0B	GETDAT	LDX	DATBUF	GET STORAGE POINTER
F9A5	D7	0D		STB	TCOUNT	
F9A7	9F	B0		STX	INDEX1	SAVE INDEX
F9A9	BE	0710		LDX	#TBUFFER	POINT TO TEMPORARY BUFFER
F9AC	0F	0E		CLR	TCHAR	
F9AE	B6	DE28		LDA	KEYPAD	CLEAR ANY RESIDUAL CHARACTER IRQ
F9B1	BD	96	DATA1	BSR	KBINCH	GET A CHARACTER
F9B3	27	4D		BEG	ERROR	ZERO BIT IS ERROR FLAG FOR KBINCH
>F9B5	17	007F		LBSR	CHARCK	CHECK FOR TIMEOUT
F9B8	0A	0D		DEC	TCOUNT	UPDATE CHAR. COUNT
F9BA	26	2E		BNE	NXTCHR	
F9BC	01	0D		CMPB	#\$0D	
F9BE	26	5A		BNE	ERROR1	LAST CHAR. MUST BE CR
F9C0	E7	B0	RET	STB	X+	
F9C2	34	40		PSHS	U	SAVE U
F9C4	1F	13		TFR	X,U	

F9C6	9E	80		LDX	INDEX1	POINT TO STORAGE AREA
F9C8	DF	80		STU	INDEX1	
F9CA	D6	0D		LDB	TCOUNT	FETCH REMAINING NUMBER OF CHAR
F9CC	27	07		BEQ	CHARS1	
F9CE	B6	30		LDA	#\$30	LOAD A WITH ASCII ZERO
F9D0	A7	80	ZEROS	STA	X+	
F9D2	5A			DECB		
F9D3	26	FB		BNE	ZEROS	
F9D5	34	20	CHARS1	PSHS	Y	SAVE Y
F9D7	108E	0710		LDY	*TBUFFR	
F9D8	A6	A0	CHARS	LDA	Y+	
F9DD	A7	80		STA	X+	
F9DF	109C	80		CMFY	INDEX1	
F9E2	27	02		BEQ	RET1	
F9E4	20	F5		BRA	CHARS	
F9E6	9F	0B	RET1	STX	DATBUF	
F9E8	35	E0		PULS	Y,U,PC	CLEAN STACK, RETURN
F9EA	C1	0D	NXTCHR	CMPB	#\$0D	IS CHAR. A CR
F9EC	26	02		BNE	NXTONE	
F9EE	20	D0		BRA	RET	
F9F0	C1	7F	NXTONE	CMPB	#\$7F	IS IT A DELETE
F9F2	26	02		BNE	CHAR	
F9F4	5F			CLRB		SHOW CANCELLATION OF ENTRY
F9F5	39			RTS		
F9F6	E7	80	CHAR	STB	X+	SAVE CHARACTER
F9F8	1F	98		TFR	B,A	
F9FA	17	050B		LBSR	WRC	ECHO CHARACTER
F9FD	58			ASLB		
F9FE	2B	4D		BMI	CMD	IF CMD, PROCESS
FA00	20	AF		BRA	DATA1	
FA02	17	04C5	ERROR	LBSR	WFS	OUTPUT STRING
FA05	49	4C 4C 45		FCC	'ILLEGAL CHARACTER!'	
FA09	47	41 4C 20				
FA0D	43	48 41 52				
FA11	41	43 54 45				
FA15	52	21				
FA17	00			FCB	0	
FA18	20	1B		BRA	WAIT	
FA1A	17	04AD	ERROR1	LBSR	WFS	
FA1D	54	30 30 20		FCC	'TOO MANY CHARACTERS!'	
FA21	4D	41 4E 59				
FA25	20	43 48 41				
FA29	52	41 43 54				
FA2D	45	52 53 21				
FA31	00			FCB	0	
FA32	17	FF14	WAIT	LBSR	KBINCH	WAIT FOR ANY CHAR. INPUT
FA35	5F			CLRB		SHOW ERROR
FA36	39			RTS		
FA37	D1	0E	CHARCK	CMPB	TCHAR	COMPARE TO PREVIOUS CHAR.
FA39	27	07		BEQ	CKMATC	
FA3B	D7	0E	NEW	STB	TCHAR	SAVE CHAR. IF NO MATCH
FA3D	86	03		LDA	#3	

```

FA3F 97 0F STA TCHCNT SET FOR THREE INPUTS OF CHAR.
FA41 39 RTS

```

```

FA42 0A 0F CKMATC DEC TCHCNT
FA44 27 F5 BEQ NEW
FA46 35 02 PULS A
FA48 35 02 PULS A
FA4A 16 FF64 LBRA DATA1

```

```

FA4D 8E FA0C CMD LDX #CMDADR GET CMD BASE ADDRESS
FA50 57 ASRB RESTORE CHAR
FA51 3A ABX
FA52 6E 84 JMP X

```

```

FA54 20 07 CMDH BRA CMDH1 HALT COMMAND ROUTINE

```

* LOCATION RUNFLG MUST BE LOADED WITH THE
* ADDRESS OF THE ROUTINE TO BE STARTED ON RUN
* COMMAND. ELSE, AN ERROR WILL BE RETURNED.

```

FA56 DC 31 CMDR LDD RUNFLG RUN COMMAND ROUTINE
FA58 27 0C BEQ ERROR2
FA5A 34 06 PSHS D PUT D INTO SUBROUTINE RETURN CALL
FA5C 39 RTS

```

* THE HALT COMMAND ENTERS A LOOP AND STAYS THERE
* UNTIL A RUN COMMAND IS RECEIVED.
* UPON RECEIPT OF THE R CMD, THE PROCESSOR WILL
* RESUME AT THE ROUTINE THAT WAS IN OPERATION
* WHEN HALT WAS CALLED. THIS IS DONE BY
* REPORTING AN ERROR AND LETTING THE ROUTINE
* USE ITS EXCEPTION CALL.

```

FA5D 17 FEE9 CMDH1 LBSR KBINCH WAIT FOR A CHARACTER
FA60 C1 4A CMPB #4A IS IT AN R?
FA62 26 F9 BNE CMDH1 IF NOT LOOP AGAIN
FA64 5F CLRB ELSE, SHOW ERROR
FA65 39 RTS AND RETURN

```

```

FA66 20 9A ERROR2 BRA ERROR

```

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

CHAR	F9F6	CHARCK	FA37	CHARS	F9DB	CHARS1	F9D5	CKMATC	FA42
CMD	FA4D	CMDADR	FA0C	CMDH	FA54	CMDH1	FA5D	CMDR	FA56
DATA1	F9B1	DATBUF	070B	ERROR	FA02	ERROR1	FA1A	ERROR2	FA66

GETDAT	F9A3	INDEX1	07B0	KBINCH	F949	KEYPAD	DE28	NEW	FA3B
NATCHR	F9EA	NXTONE	F9F0	RET	F9C0	RET1	F9E6	RUNFLG	0731
BUFFR	0710	TCHAR	070E	TCHCNT	070F	TCOUNT	070D	WAIT	FA32
WFL	FECA	WRC	FF0B	ZEROS	F9D0				

NO SUCH FILE

* CLRBUF

* THIS ROUTINE CLEARS AREAS OF MEMORY IN THE AS
* SYSTEM. THE STARTING AND ENDING ADDRESSES ARE TO
* BE PLACED IN THE LOCATIONS INDICATED, BY THE
* CALLING PROGRAM. A AND X ARE DESTROYED.

```

07DB          ORG      $07DB
              0007     SETDP  $07

07DB          TBUFST  RMB   2      START ADDRESS TO BE HERE
07DA          TBUFND  RMB   2      END ADDRESS TO BE HERE

FA69          ORG      $FA69

FA69 34      40      PSHS   U      SAVE U REGISTER
FA6B DE      DA      LDU    TBUFND  LOAD U WITH END ADDRESS
FA6D 4F
FA6E 36      02      NEXT   PSHU   A      STORE A IN LAST LOCATION
FA70 1193    DB      CMPU   TBUFST  HAVE WE DONE ALL
FA73 26      F9      BNE    NEXT   LOOP IF NOT DONE
FA75 36      02      PSHU   A
FA77 35      C0      PULS   U,PC   RESTORE U, RETURN

              END

```

0 ERROR(S) DETECTED

SYMBOL TABLE:

NEXT FA6E TBUFND 07DA TBUFST 07DB

* BIN2BCD

* THIS ROUTINE CONVERTS A 16 BIT BINARY
* NUMBER TO BCD AND STORES THE RESULTING
* 5 CHARACTERS.
* ON START, D CONTAINS THE BINARY NUMBER,
* AND X CONTAINS THE POINTER TO DECIMAL
* STORAGE

* SYSTEM EQUATES

FA79 K10K EQU \$FA79

* TEMPORARY STORAGE

073E ORG \$073E

073E SAVEA RMB 1 ACCUMULATOR A
073F SAVEX RMB 2 STORE DATA POINTER
0741 SAVEX1 RMB 2 POINTER TO CONSTANTS

0007 SETDP \$07

FAB1 ORG \$FAB1

FAB1 9F 3F CVBTD STX SAVEX SAVE DATA POINTER
FAB3 8E FA79 LDX #K10K POINT TO CONSTANTS
FAB6 0F 3E CVDEC1 CLR SAVEA INITIALIZE DEC CHAR
FAB8 A3 B4 CVDEC2 SUBD X
FABA 25 04 BCS CVDEC5 OVERFLOW
FABC 0C 3E INC SAVEA INC CHAR BEING BUILT
FABE 20 FB BRA CVDEC2

FAC0 E3 B4 CVDEC5 ADDD X RESTORE PARTIAL RESULT
FAC2 36 02 PSHU A SAVE A REGISTER
FAC4 9F 41 STX SAVEX1
FAC6 9E 3F LDX SAVEX POINT TO STORAGE FOR RESULT
FAC8 96 3E LDA SAVEA
FACA BB 30 ADDA #\$30 MAKE ASCII CHARACTER
FACC A7 B4 STA X
FACE 37 02 PULU A RESTORE A REGISTER
FAD0 30 01 LEAX 1,X INCREMENT X
FAD2 9F 3F STX SAVEX
FAD4 9E 41 LDX SAVEX1 POINT TO CONSTANTS
FAD6 30 02 LEAX 2,X
FAD8 8C FAB3 CPX #K10K+10 ARE WE DONE
FADB 26 D9 BNE CVDEC1
FADD 39 RTS

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

CVBTD	FAB1	CVDEC1	FAB6	CVDEC2	FABB	CVDEC5	FAC0	K10K	FA79
SAVEA	073E	SAVEX	073F	SAVEX1	0741				

* BCD2BIN
* THIS ROUTINE CONVERTS A STRING OF 5
* ASCII NUMBERS TO A 16 BIT BINARY VALUE.
* THE INITIAL STRING SHOULD NOT EXCEED
* 65,535.
* X SHOULD POINT TO THE START OF THE
* ASCII STRING.
* THE RESULT WILL BE IN D.

* TEMPORARY STORAGE

073A		ORG	\$073A	
073A	TEMP	RMB	1	BCD STORAGE
073B	TEMP1	RMB	2	BINARY STORAGE
073D	COUNT	RMB	1	STORAGE FOR CHARACTER COUNT
	0007	SETDF	\$07	

* CONSTANTS

FA79		ORG	\$FA79	
FA79	2710	K10K	FDB	10000
FA7B	03EB		FDB	1000
FA7D	0064		FDB	100
FA7F	000A		FDB	10
FAB1	0001		FDB	1
FA83	0F 3A	CVDTB	CLR	TEMP
FA85	0F 3B		CLR	TEMP1
FA87	0F 3C		CLR	TEMP1+1
FA89	10BE FA79		LDY	#K10K
FA8D	86 05		LDA	#\$05
FA8F	97 3D		STA	COUNT
FA91	5F	NEXT	CLRB	
FA92	A6 B0		LDA	X+
FA94	B0 30		SUBA	#\$30
FA96	27 0E		BEQ	SUM
FA98	97 3A		STA	TEMP
FA9A	4F		CLRA	
FA9B	5F		CLRB	
FA9C	E3 A4	CV	ADDD	Y
FA9E	0A 3A		DEC	TEMP
FAA0	26 FA		BNE	CV
FAA2	D3 3B		ADDD	TEMP1
FAA4	DD 3B		STD	TEMP1
FAA6	0A 3D	SUM	DEC	COUNT
FAA8	27 04		BEQ	EXIT
FAAA	31 22		LEAY	2,Y
FAAC	20 E3		BRA	NEXT

```
FAAE DC 3B EXIT LDD TEMP1
FAB0 39 RTS
END
```

0 ERROR(S) DETECTED

SYMBOL TABLE:

COUNT	073D	CV	FA9C	CVDTB	FAB3	EXIT	FAAE	K10K	FA79
NEXT	FA91	SUM	FAA6	TEMP	073A	TEMP1	073B		

* FIRQHDL

* THIS ROUTINE IS AN INTERRUPT HANDLER FOR FIRQ
* WHICH CHOOSES BETWEEN A JUMP TO MONITOR AND
* A REPEAT ROUTINE. SELECTION IS MADE BY
* MEANS OF THE STATUS OF THE FUNCT SWITCH ON THE
* PANEL OF THE PORTABLE INSTRUMENT. THE FIRQ IS
* ISSUED BY PRESSING THE KEY MARKED RPT(MONITOR).

* SYSTEM EQUATES

07F6 EFIN EQU \$07F6 STORAGE LOCATION FOR FIRQ VECTOR
DE2A FRQFLG EQU \$DE2A PIA B SIDE DATA REGISTER
FC3C NMI EQU \$FC3C ENTRY ROUTINE FOR AS01
0700 INDEX EQU \$0700

0733 ORG \$0733

0007 SETDP \$07

0733 RUNCNT RMB 1 NUMBER OF REPEATS PERFORMED
0734 RPTADR RMB 2 ADDRESS TO WHICH REPEAT GOES

FADE ORG \$FADE

* INITIALIZATION

FADE 9F 00 FRQINZ STX INDEX SAVE X
FAE0 8E FAF1 LDX #FRQVEC GET ADDRESS FOR FIRQ ROUTINE
FAE3 36 10 PSHU X SAVE IN STACK
FAE5 8E FC3C LDX #NMI POINT TO MONITOR
FAE9 9F 34 STX RPTADR SAVE AS DEFAULT FIRQ
FAEA 9E 00 LDX INDEX
FAEC 36 32 PSHU Y,X,A
FAEE 1C 0F ANDCC #\$0F ENABLE FIRQ
FAF0 39 RTS

* INTERRUPT HANDLER

FAF1 F6 DE2A FRQVEC LDB FRQFLG READ PIA FOR FUNCTION FLAG
FAF4 2A 06 BPL REPEAT IF BIT7 = 0 REPEAT ROUTINE
FAF6 8E FC3C DEBUG LDX #NMI DO MONITOR STARTUP
FAF9 AF 61 STX 1,S SET LOCATION TO JUMP TO
FAFB 3B RTI JUMP TO AS01
FAFC 0C 33 REPEAT INC RUNCNT
FAFE 6E 9F 0734 JMP [RPTADR]

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

DEBUG	FAF6	EFIN	07F6	FRQFLG	DE2A	FRQINZ	FADE	FRQVEC	FAF1
INDEX	0700	NMI	FC3C	REPEAT	FAFC	RPTADR	0734	RUNCNT	0733

* STARTUP

* THIS ROUTINE IS ENTERED WHEN RESET IS RECEIVED BY
* THE ADAPTIVE SCIENCE SYSTEM. IT PERFORMS ALL
* REQUIRED INITIALIZATIONS, AND THEN POINTS TO THE
* START OF THE ROUTINE, AND WAITS FOR A RUN COMMAND

* SYSTEM EQUATES

FB00	INTIME	EQU	\$FB00	INITIALIZE TIMER
FB40	INITAD	EQU	\$FB40	INITIALIZE A TO D
FB9D	INITDA	EQU	\$FB9D	INITIALIZE D TO A
F93C	INITKP	EQU	\$F93C	INITIALIZE KEYPAD
07D8	TBUFST	EQU	\$07D8	
07DA	TBUFND	EQU	\$07DA	
FC00	RES	EQU	\$FC00	INITIALIZE MONITOR AND ACIA
FADE	FRQINZ	EQU	\$FADE	SET UP FIRQ ROUTINE
FBF0	SAVECK	EQU	\$FBF0	CMOS MEMORY SAVE CHECK
070A	SAVFLG	EQU	\$070A	
FA69	CLRBUF	EQU	\$FA69	
8010	BEGDAT	EQU	\$8010	START OF CMOS DATA STORAGE
0743	STARTD	EQU	\$0743	
0731	RUNFLG	EQU	\$0731	
F949	KBINCH	EQU	\$F949	
FA56	CMDR	EQU	\$FA56	
8002	SAVSTO	EQU	\$8002	POINTER TO CMOS DATA STORAGE
F000	BEGIN	EQU	\$F000	LOCATION FOR START OF
				SEQUENCE

~~* 308260 EQU AF600~~

0007 SETDP \$07

FB1F ORG \$FB1F

FB1F	86	20	STARTUP	PSHU	Y	
FB21	8D	BB		BSR	FRQINZ	
FB23	86	07		LDA	#\$07	
FB25	1E	BB		EXG	A,DF	
FB27	17	FCD6		LBSR	INTIME	
FB2A	17	FE70 FB33		LBSR INITDA	54036	
FB2D	17	FD13		LBSR	INITAD	
FB30	17	FE09		LBSR	INITKP	
FB33	8E	0000		LDX	#\$0000	
FB36	9F	DB		STX	TBUFST	POINT TO START OF SCRATCHPAD
FB38	8E	07D7		LDX	#\$07D7	
FB3E	9F	DA		STX	TBUFND	POINT TO END OF SCRATCHPAD
FB3D	17	FF29		LBSR	CLRBUF	
FB40	8E	0E00		LDX	#\$0E00	
FB43	9F	DB		STX	TBUFST	POINT TO DATA STORAGE
FB45	8E	0FFF		LDX	#\$0FFF	
FB48	9F	DA		STX	TBUFND	POINT TO END OF DATA STORAGE
FB4A	17	FF1C		LBSR	CLRBUF	
FB4D	17	FDA0		LBSR	SAVECK	
FB50	0D	0A		TST	SAVFLG	HAS CMOS MEMORY BEEN PROTECTED?
FB52	26	20		BNE	SAVDAT	YES, GET START OF UNPROTECTED AREA

```

FB54 BE    B010          LDX    #BEGDAT
FB57 9F    43           STX    STARTD      SAVE POINTER TO DATA AREA
FB59 9F    D8           STX    TBUFST      CLEAR CMOS MEM.
FB5B 8E    B7FF          LDX    #BEGDAT+$7EF
FB5E 9F    DA           STX    TBUFND
FB60 17    FF06          LBSR   CLRBUF
FB63 CC    F000          GO     LDD    #BEGIN
FB66 DD    31           STD    RUNFLG      POINT TO PROGRAM ENTRY
FB68 17    FDDE          GETR   LBSR   KBINCH
FB6B C1    4A           CMPB  #4A
FB6D 26    F9           BNE   GETR        IF CHARACTER NOT R LOOP
FB6F 17    FEE4          LBSR   CMDR
FB72 27    AB           BEQ   STARTUP     TRY AGAIN, IF ERROR

FB74 BE    B002          SAUDAT LDX    SAUSTO   GET NEXT DATA LOCATION
FB77 9F    43           STX    STARTD     STORE IN POINTER
FB79 20    EB           BRA   GO

```

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

BEGDAT	B010	BEGIN	F000	CLRBUF	FA69	CMDR	FA56	FRQINZ	FADE
GETR	FB68	GO	FB63	INITAD	FB43	INITDA	FB9D	INITKP	F93C
INTIME	FB00	KBINCH	F949	RES	FC00	RUNFLG	0731	SAUDAT	FB74
SAVECK	FBF0	SAUFLG	070A	SAUSTO	B002	STARTD	0743	STARTU	FB1F
TBUFND	07DA	TBUFST	07DB						

* PGMSAVE

* THIS ROUTINE WILL DISABLE AND ENABLE ACCESS
* TO THE CMOS MEMORY WHILE THE PORTABLE UNIT
* IS POWERED UP, TO RETAIN MEMORY DURING
* POWER OFF, THE SAVE BUTTON MUST BE DEPRESSED

* SYSTEM EQUATES

DE2A ORB EQU \$DE2A DATA REGISTER PIA B SIDE

FB7D ORG \$FB7D

FB7D CC 7F04 PGMSAV LDD #\$7F04 DISABLE CMOS MEMORY
FB80 7F DE2B CLR ORB+1 CLEAR CONTROL REGISTER B
FB83 FD DE2A STD ORB SET B SIDE BIT 7-IN, REST-OUT
FB86 86 3F LDA #\$3F
FB88 B7 DE2A STA ORB SET BIT 6 LO
FB8B 39 RTS

FB8C 86 7F UNSAVE LDA #\$7F
FB8E B7 DE2A STA ORB SET BIT 6 HI
FB91 39 RTS

FB92 CC 3F04 EXT LDD #\$3F04 RETURN TO EXTERNAL CONTROL
FB95 7F DE2B CLR ORB+1 CLEAR CONTROL REGISTER B
FB98 FD DE2A STD ORB SET B SIDE 2-IN 6-OUT
FB9B 39 RTS

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

EXT FB92 ORB DE2A PGMSAV FB7D UNSAVE FB8C

* UN/PACK

* THIS ROUTINE PACKS FOUR 6 BIT CHARACTERS(ASCII)
* INTO THREE 8 BIT BYTES, OR UNPACKS THREE EIGHT
* BIT BYTES INTO FOUR BYTES. RECONVERSION TO ASCII
* IS ALSO DONE. ON ENTRY*
* FOR PACKING, X POINTS TO THE START OF DATA
* Y POINTS TO THE START OF STORAGE
* D CONTAINS THE NUMBER OF 4 CHAR BLOCKS

* FOR UNPACK, X CONTAINS THE START OF STORAGE
* Y CONTAINS THE START OF CHAR. STORAGE
* D CONTAINS THE NUMBER OF 4 CHAR BLOCKS

FB9C		ORG	\$FB9C	
FB9C	4C			PACKS INCA ADJUST COUNT OF MS BYTE
FB9D	34	06	PSHS D	PUT COUNT ON THE STACK
FB9F	2D	0A	PAC1 BSR PACK	PACK 4 INTO 3
FBA1	6A	61	DEC 1,3	LS COUNT
FBA3	26	FA	BNE PAC1	
FBA5	6A	E4	DEC 0,3	MS BYTE
FBA7	26	F6	BNE PAC1	
FBA9	35	B6	PULS D,PC	CLEAN UP STACK,RETURN
FBAB	EC	B1	PACK LDD X++	GET FIRST TWO CHARACTERS
FBAD	58		ASLB	
FBAE	58		ASLB	
FBAF	58		ASLB	
FBB0	49		ROLA	
FBB1	58		ASLB	
FBB2	49		ROLA	
				* ACCA IS NOW PACKED AND ACCB CONTAINS 4 BITS * LEFT JUSTIFIED
FBB3	A7	A0	STA Y+	STORE FIRST PACKED BYTE
FBB5	A6	B0	LDA X+	GET THIRD CHAR.
FBB7	44		LSRA	
FBB8	44		LSRA	
FBB9	B4	0F	ANDA #\$0F	CLEAN UP MS NYBBLE
				* ACCA HAS MS NYBBLE AND ACCB HAS LS NYBBLE
FBBE	34	04	PSHS B	PUT B IN TEMP STORAGE
FBD0	AA	E0	ORA S+	PUT CHAR TOGETHER, CLEAN STACK
FBD2	A7	A0	STA Y+	STORE SECOND PACKED BYTE
FBD4	EC	B1	LDD X++	GET LAST TWO CHAR.
				* PICK UP 2 LSB FROM A AS 2 MSB IN B
FBD3	58		ASLB	
FBD4	58		ASLB	

```

FBC5 44          LSRA
FBC6 56          RORB
FBC7 44          LSRA
FBC8 56          RORB
FBC9 E7  A0     STB   Y+      STORE THIRD PACKED BYTE
FBC8 39          RTS

```

```

FBC0 34  20     UNPAKS  PSHS  Y
FBC0 4C          INCA          ADJUST COUNTER MS BYTE
FBCF 34  06     UNP1    PSHS  D      PUT COUNT ON THE STACK
FBD1 8D  0A     UNP1    BSR   UNPACK UNPACK 3 INTO 4
FBD3 6A  61     UNP1    DEC   1,S    LS COUNT
FBD5 26  FA     UNP1    BNE   UNP1
FBD7 6A  E4     UNP1    DEC   S      MS COUNT
FBD9 26  F6     UNP1    BNE   UNP1
FBD8 35  A6     UNP1    PULS  D,Y,PC CLEANSTACK, RETURN

```

* UNPACK RETURNS FOUR RIGHT-JUSTIFIED 6-BIT
* CHARACTERS FROM THREE PACKED 8-BIT BYTES

```

FBDD 34  06     UNPACK  PSHS  D      SAVE D REGISTER
FBDF EC  80     UNPACK  LDD   X+
FBE1 44          UNPACK  LSRA          :
FBE2 56          UNPACK  RORB          : 16-BIT SHIFT, TWO PLACES
FBE3 44          UNPACK  LSRA          :
FBE4 56          UNPACK  RORB          :

```

* ACCA IS NOW UNPACKED

```

FBE5 54          UNPACK  LSRB
FBE6 54          UNPACK  LSRB

```

* ACCB IS NOW UNPACKED

```

FBE7 ED  A1     UNPACK  STD   Y++     STORE 1ST AND 2ND CHARS
FBE9 EC  B0     UNPACK  LDD   X+     GET 2ND AND THIRD BYTES
FBEB 58          UNPACK  ASLB          :
FBEC 49          UNPACK  ROLA          : ANOTHER SHIFT, TWO PLACES
FBED 58          UNPACK  ASLB          :
FBEF 49          UNPACK  ROLA          :
FBF0 B4  3F     UNPACK  ANDA  ##3F    CLEAR TOP 2 BITS

```

* ACCA IS NOW UNPACKED

```

FBF1 E6  B0     UNPACK  LDB   X+     GET 3RD BYTE AGAIN
FBF3 C4  3F     UNPACK  ANDB  ##3F

```

* BOTH ARE NOW UNPACKED

```

FBF5 ED  A1     UNPACK  STD   Y++     STORE THIRD AND FOURTH CHARS
FBF7 35  B6     UNPACK  PULS  D,PC    RECOVER D, RETURN

```

END

0 ERROR(S) DETECTED

SYMBOL TABLE:

PAC1	FB9F	PACK	FBAB	PACKS	FB9C	UNP1	FBD1	UNPACK	FBDD
UNPAKS	FBCC								

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10. SUPPLEMENTARY NOTES FHWA Contract Manager: Y. P. Virmani <input type="checkbox"/> Document describes a computer program; SF-185, FIPS Software Summary, is attached.			
11. ABSTRACT <i>(A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey, mention it here)</i> <p>The progress on a research program directed at developing a nondestructive method for measuring the corrosion of steel in concrete as related to bridge deck deterioration is reported. This report summarizes the past work and describes the new developments on this project. The five phases described are: 1) a literature review, 2) preliminary studies, 3) measurements in concrete, 4) field measurements, and 5) development of a microprocessor system.</p>			
12. KEY WORDS <i>(Six to twelve entries; alphabetical order; capitalize only proper names; and separate key words by semicolons)</i> Bridge deck corrosion; corrosion in concrete; corrosion of steel, polarization technique; rebar corrosion.			
13. AVAILABILITY <input checked="" type="checkbox"/> Unlimited <input type="checkbox"/> For Official Distribution. Do Not Release to NTIS <input type="checkbox"/> Order From Superintendent of Documents, U.S. Government Printing Office, Washington, D.C. 20402. <input checked="" type="checkbox"/> Order From National Technical Information Service (NTIS), Springfield, VA. 22161		14. NO. OF PRINTED PAGES 86	15. Price \$11.50

